NATIONAL RADIO ASTRONOMY OBSERVATORY Green Bank, West Virginia

ELECTRONICS DIVISION INTERNAL REPORT NO. 2

THE ELECTRON BEAM PARAMETRIC AMPLIFIER By DEWEY ROSS and ROBERT HAAS

SEPTEMBER 1962

NUMBER OF COPIES: 15
Rerun 11/10/66: 50 copies

THE ELECTRON BEAM PARAMETRIC AMPLIFIER

The information contained herein covers the practical application of the Adler tube since it was returned from Zenith in March where the following modifications were made.

The input and output connectors have a "c" clamp to keep the inner conductor from moving the coupling loop. Micrometers were added to give an indication of mechanical alignment of the input and output couplers. End bell clamping assembly was modified to allow more precise positioning of the R. F. capsule in the magnet. Both tubes were checked; tube 333 was erratic and had to be reconditioned. The DC block and pump balun were modified to operate above ground, and a change was made in the power supply unit here and this was noted on the schematic.

Noise temperatures measured higher than those specified by Zenith. However, their measurements were made with an automatic noise figure indicator while the ones measured here by the Y-factor method, using an Argon tube and hot-cold source.

Stability tests with tube 334-R -- noise temperature of 140 °K and 40 db gain -- show approximately .3 °K peak-to-peak noise with 15 second integration time. Changes in room temperature are quite evident on the output record. By the process of elimination, the quadrapole voltage and magnet seem quite sensitive to such changes. Pump frequency and output seem to be constant with temperature change but both are quite critical to the proper alignment for obtaining best noise temperature of the EBPA. The magnet supply uses two Kepco power supplies in series. This modification was made by D. Durand and has good stability once warm-up has been obtained.

Variation of Adler Tube Noise Temperature With Operating Parameters

The results of measurements made on the noise temperatures of two Adler tubes between June 21 and September 15, 1962 are shown on the accompanying graphs.

In addition, to the plotted parameters, the interception current was also monitored. It was found that lowest noise temperatures and best stability occurred

simultaneously with low interception current. The interception current is monitored at the cuccia couplers and is used as an indication of proper beam position. Any mismatch or improper voltages and currents change the beam position and therefore induces a current into the plates of the couplers. Therefore, in beginning measurements after installing the tube, the best procedure is to adjust the mechanical adjustments for minimum interception current and the electrical adjustments as per the manufacturer's specifications. This will bring the noise temperature within a range readable on the Automatic Noise Figure Indicator. Once this is achieved, the system can be adjusted for lowest noise temperature directly. It was found that it is possible to get very close to the proper mechanical adjustment, local oscillator frequency, and mixer current on the first try. Following this, lowest noise temperature is achieved by cyclic adjustment of the other electrical parameters with occasional modification of the above-mentioned three. Once a low noise temperature was achieved, it remained constant over long periods of time (days). In fact, the distrubing factors were usually external to the tube, such as equipment failures or changes in the measurement program.

As can be seen from the attached graphs, the noise temperature is extremely sensitive to changes in the tube voltages, currents, and frequencies, and the Quadrapole voltage being the most critical and Electrode B Voltage being the least critical. The critical parameters are usually adjusted very close to the brink of noise temperature degeneration. If they are set too close to the drop off point, slight instabilities, in power supply or room temperature for instance, will cause a degradation in noise temperature.

The gain vs. pump power and noise temperature vs. pump power measurements show that the Rhode and Swartz SLRD is not as stable as the FXR pump. However, one should consider the fact that during the two above-mentioned measurements the pump had to be turned off and on, and therefore the stability would not be as good.

The two tubes showed similar characteristics as far as sensitivity to parameter change, but tube 233-R gave a much lower noise temperature (100°) than did tube 234-R (140°).

Voltages and Currents for Adler Tube 234-R

These are the values which are held constant while one at a time is varied for the following curves. (Noise temperature is measured with Hot-Cold Noise Source.)

A = 25.1 V

B = 14.5 V

CC = 11.4 V

Q = 7.3 V

Mag = 1.25 A (on PS No. 1312)

Call = $29 \mu A$

Cath = 0+ (inception current)

Mixer = 1 mA

L/O = 1451 Mc

Pump = 2832.5 Mc

Mag Volts = PS 1312: 38 V

PS : 31 V

NT with above settings = 160 °K - 165 °K

Voltages and Currents for Adler Tube 233-R

A = 26.2 V

B = 18.0 V

CC = 8.7 V

Q = 6.4 V

Mag = 1.255

Call = $18.5 \mu A$

Cath = 12.6 mA

Inc = $0.5 \mu A$

Mixer = 1 mA

L/O = 1435 Mc

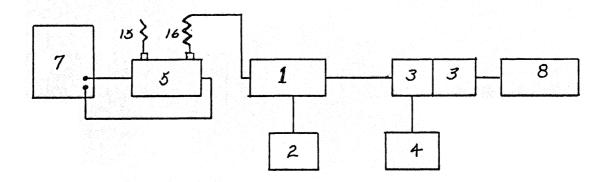
Pump = 2809.5 Mc

NT with above settings = 110 °K - 130 °K

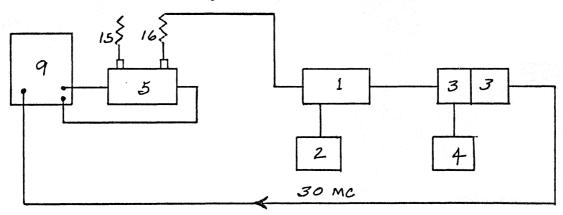
The following block diagrams describe the systems used in making the various measurements. A description of components is attached.

I. Noise Figure Measurements

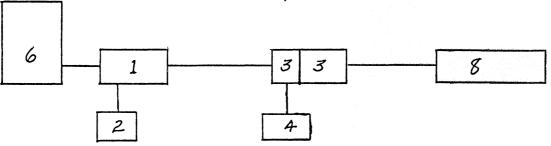
A. Y-Factor Method (Argon)



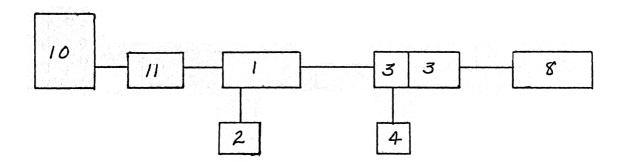
B. Automatic Method



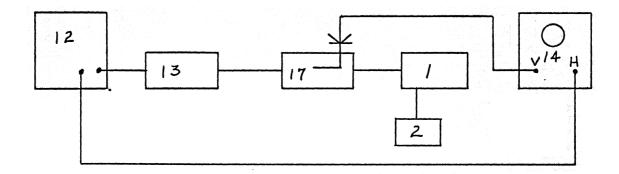
C. Hot-Cold, Y-Factor Method



II. Gain Measurements

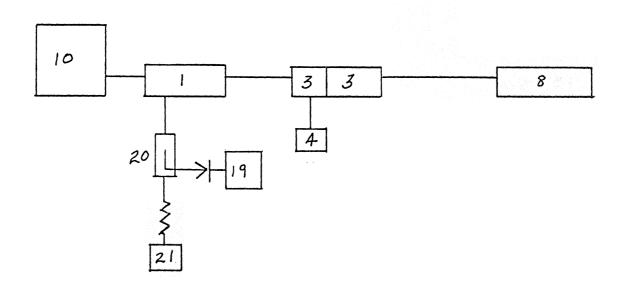


III. Coupler Alignment

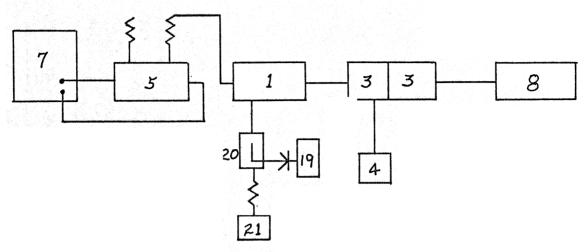


- A. Input coupler adjusted with voltages applied.
- B. Output coupler adjusted without voltages applied.

IV. Gain Measurement as a Function of Pump Power

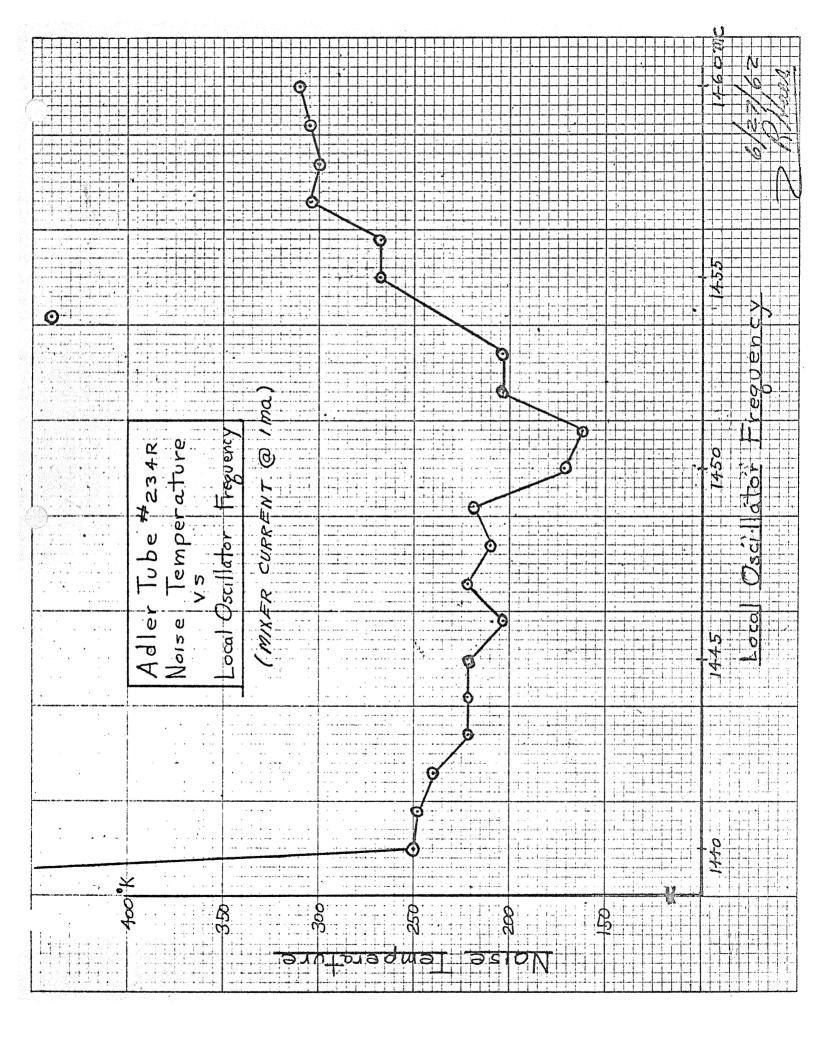


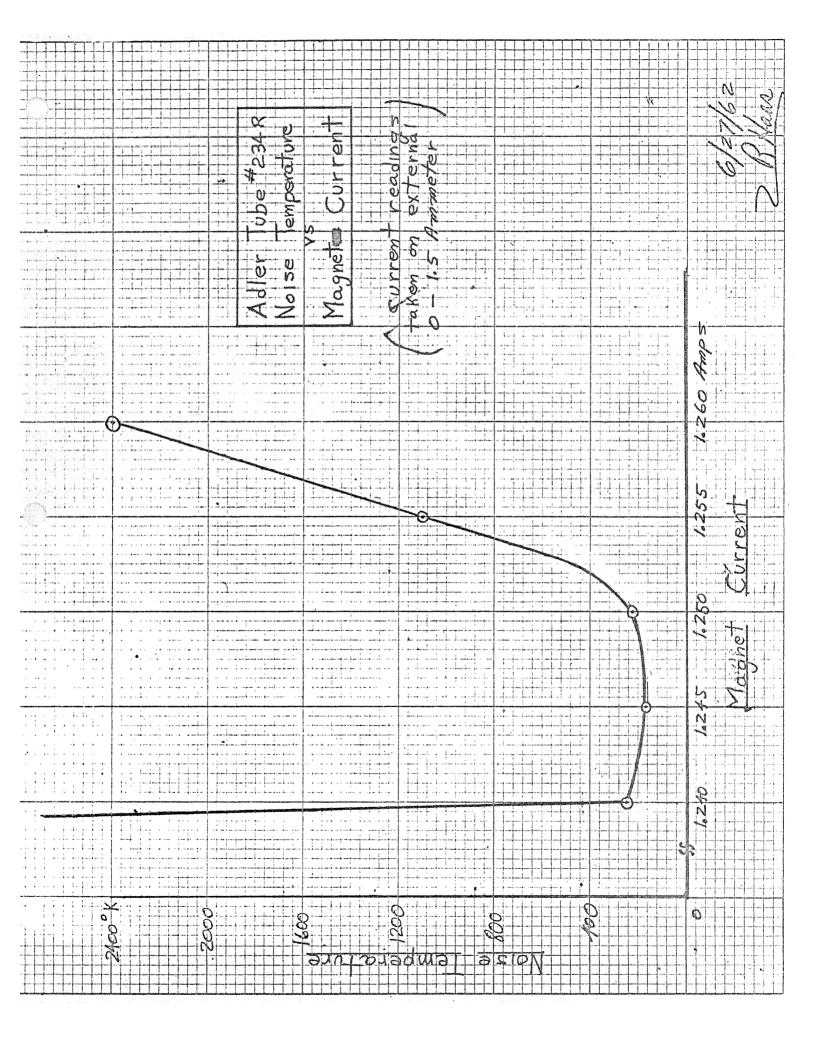
V. Noise Measurements as a Function of Pump Power

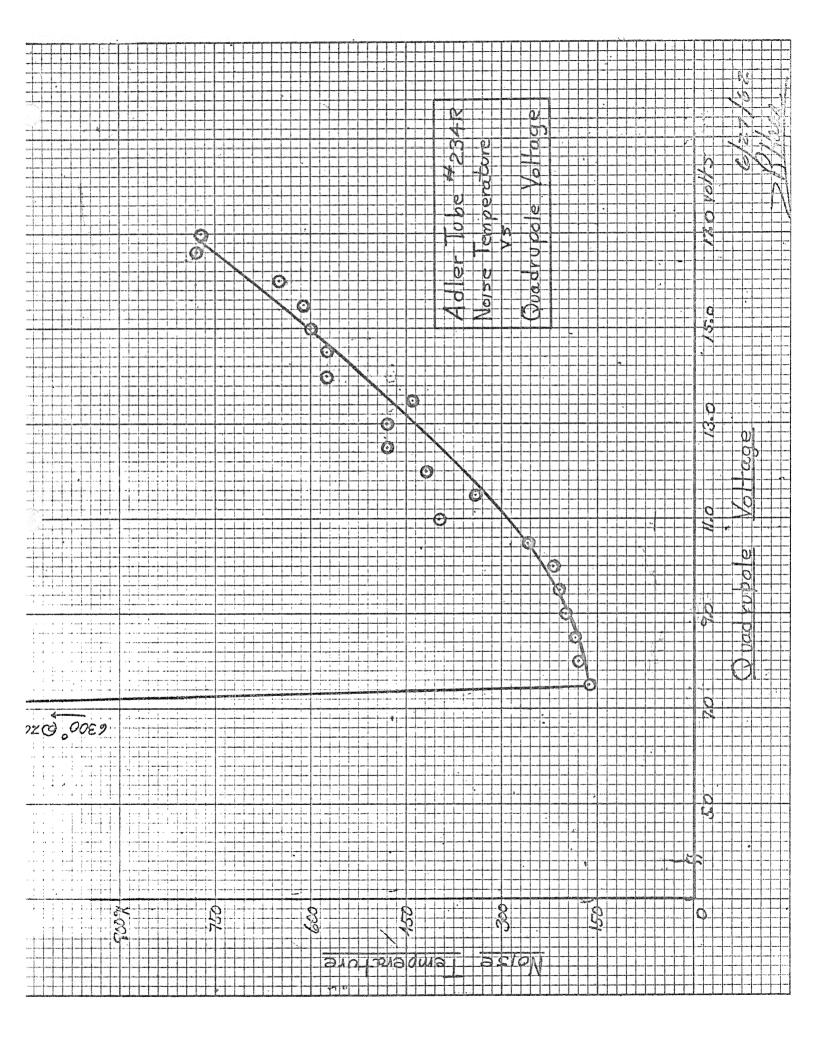


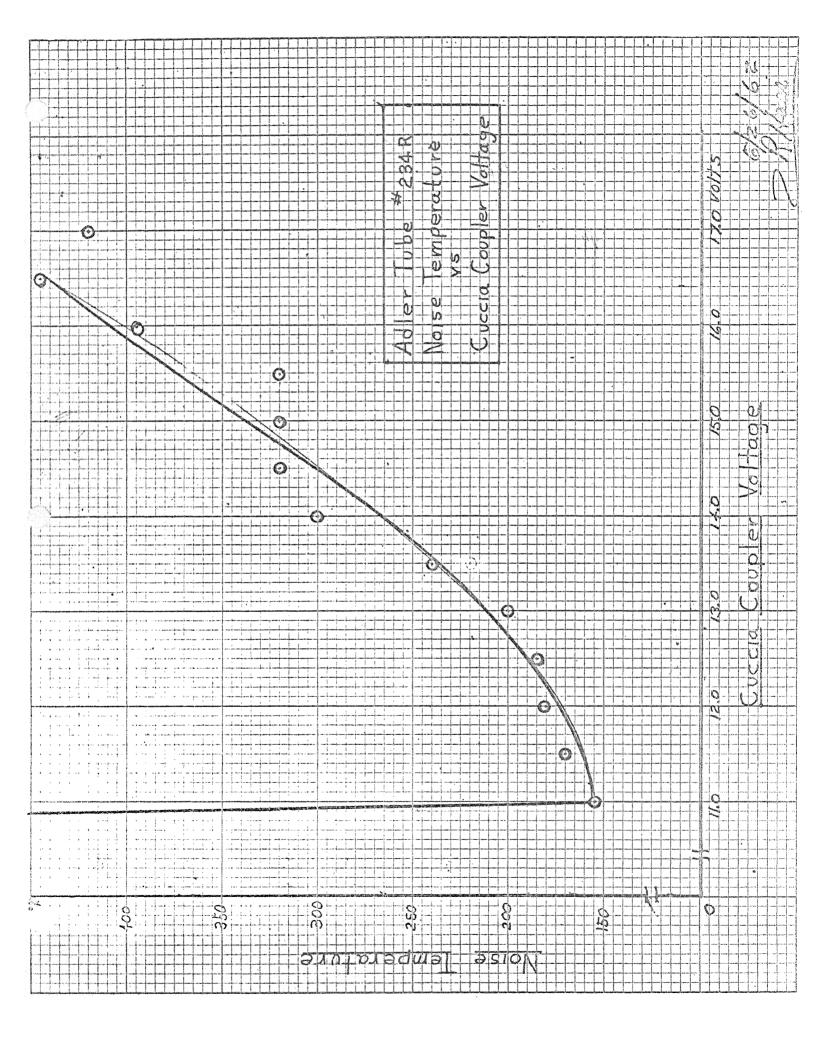
Components Used in Measurement

1.	EBPA	
2.	Pump	FXR Model S772A
3.	Mixer-Preamplifier	LEL Model LAC-3
4.	L.O.	GR Model 1218-A
5.	Noise Source (Argon)	AIL Model 7010
6.	Noise Source, Hot-Cold	AIL Model 70
7.	Noise Source, Power Supply	AIL Model 71
8.	Test Receiver	AIL Model 132
9.	Automatic Noise Figure Indicator	HP Model 340B
10.	Signal Generator	HP Model 614A
11.	Isolator	Melabs Model RL-1
12.	Sweep Generator	HP Model 682C
13.	Frequency Meter, Cavity	FXR Model N410A
14.	Scope	
15.	50	
16.	10 db Attenuator	
17.	Directional Coupler	
18.	Crystal Detector	
19.	Power Meter and Bolometer	HP Model 431A
20.	Directional Coupler	
21.	Pump	Rhode & Swartz SLRD

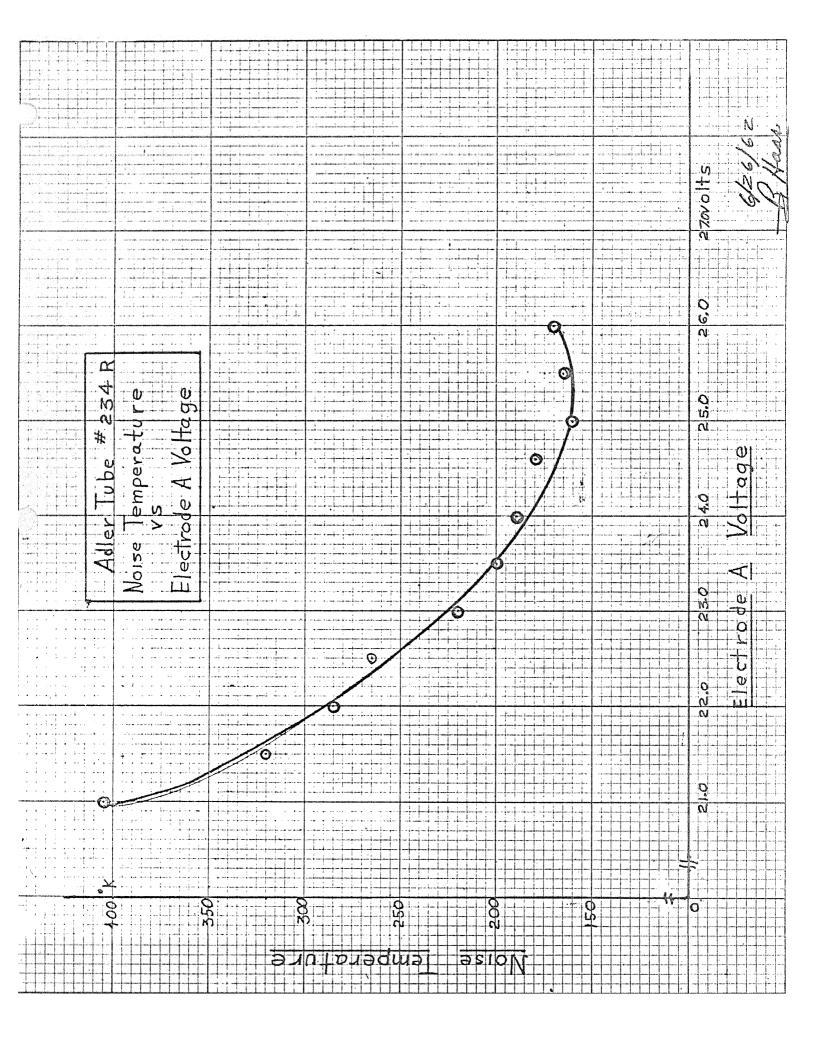


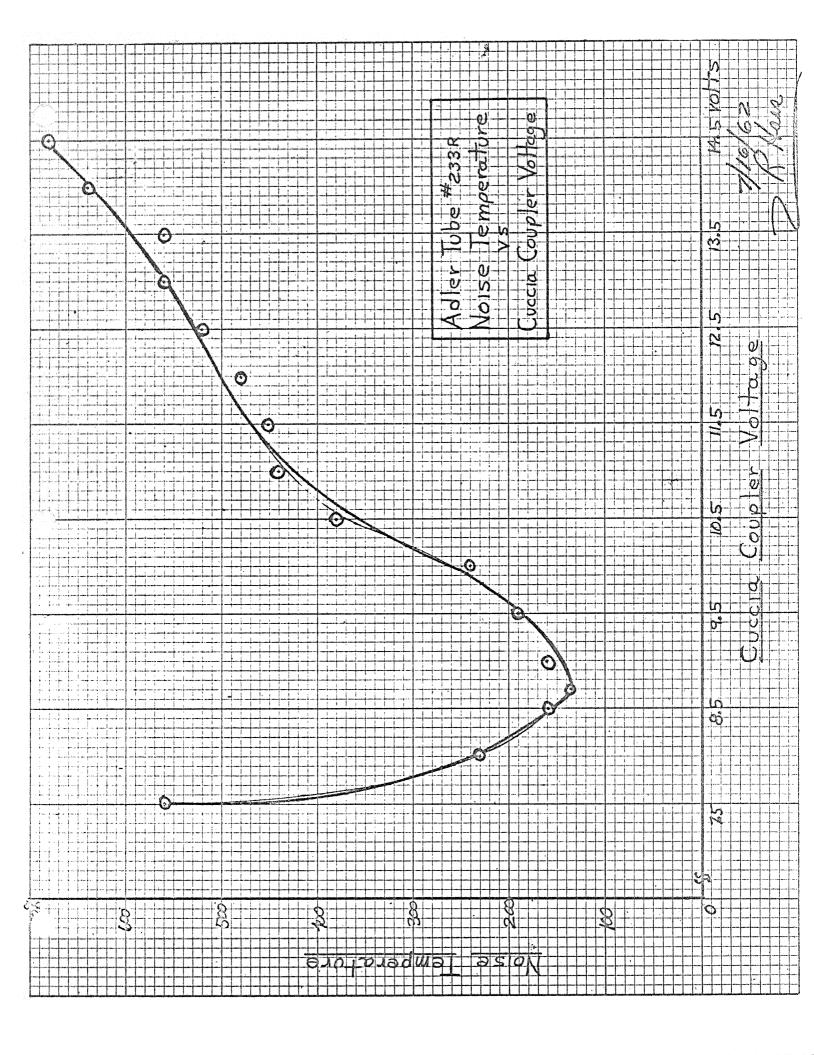


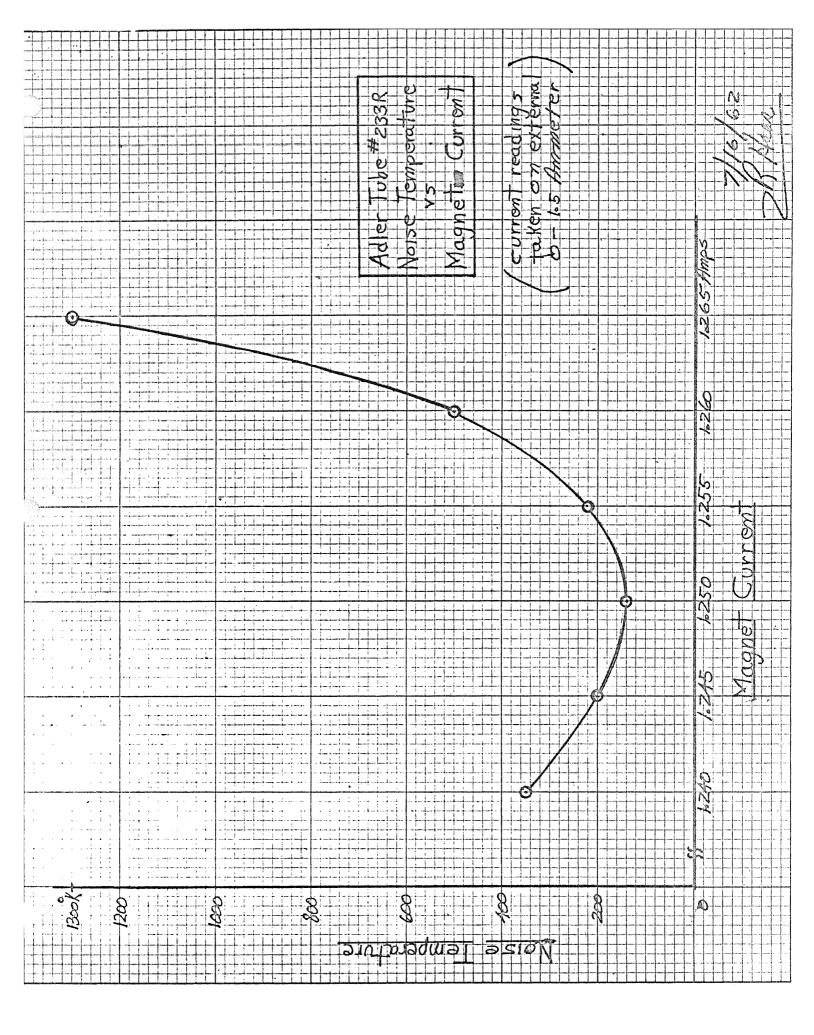


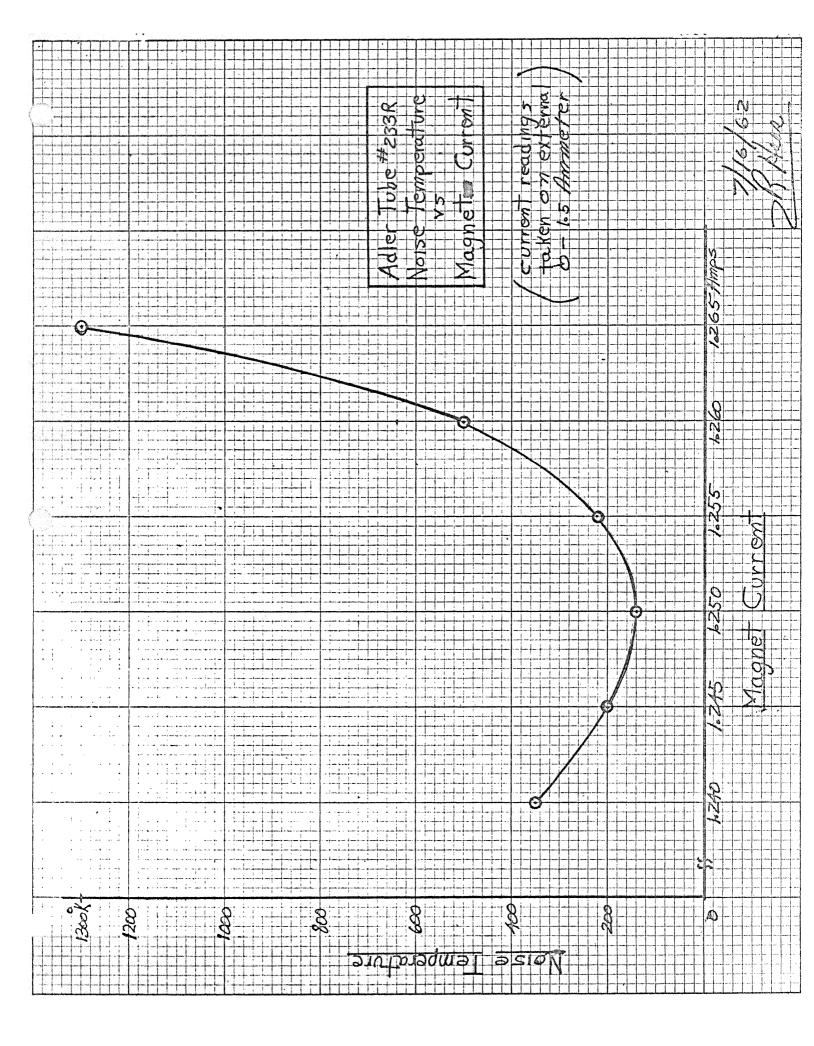


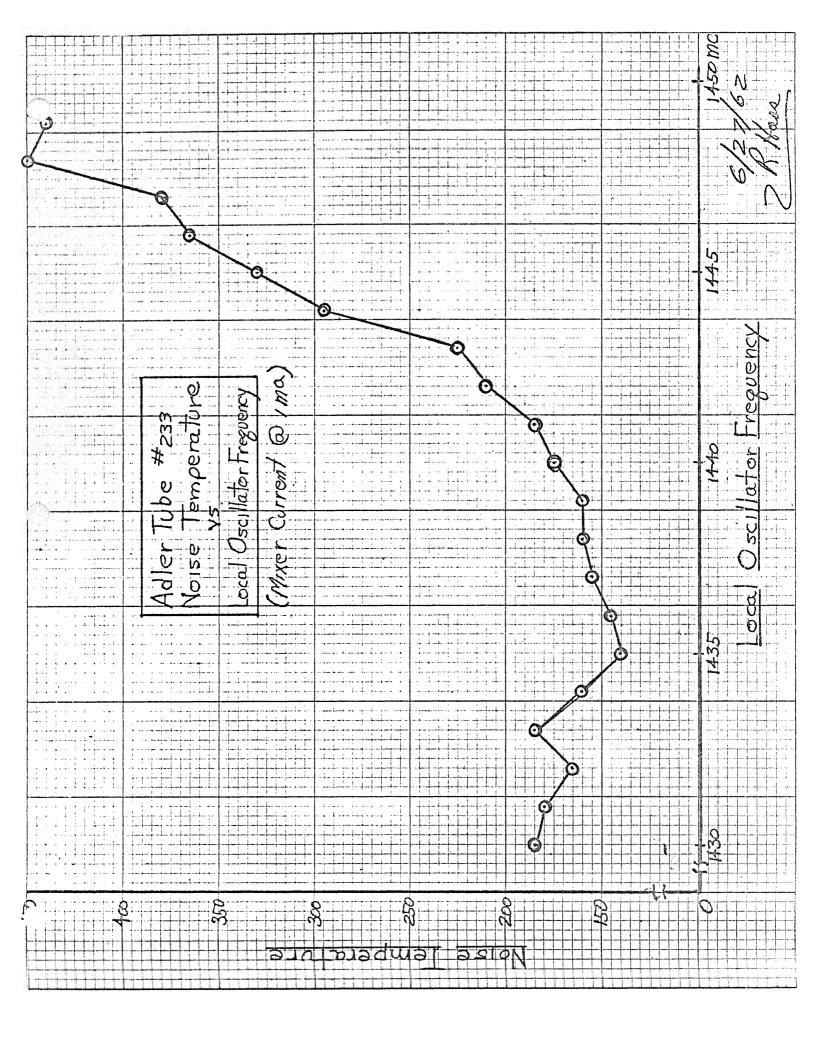
Adler Tube 234R Noise Temperature	Electrode B Voltage	•	0			13.0 IS.0
)			A second of the	700 1100 1100 1100 1100 1100 1100 1100
· 8	350 Fe	utorega	26 <u>L</u> GN	3		O

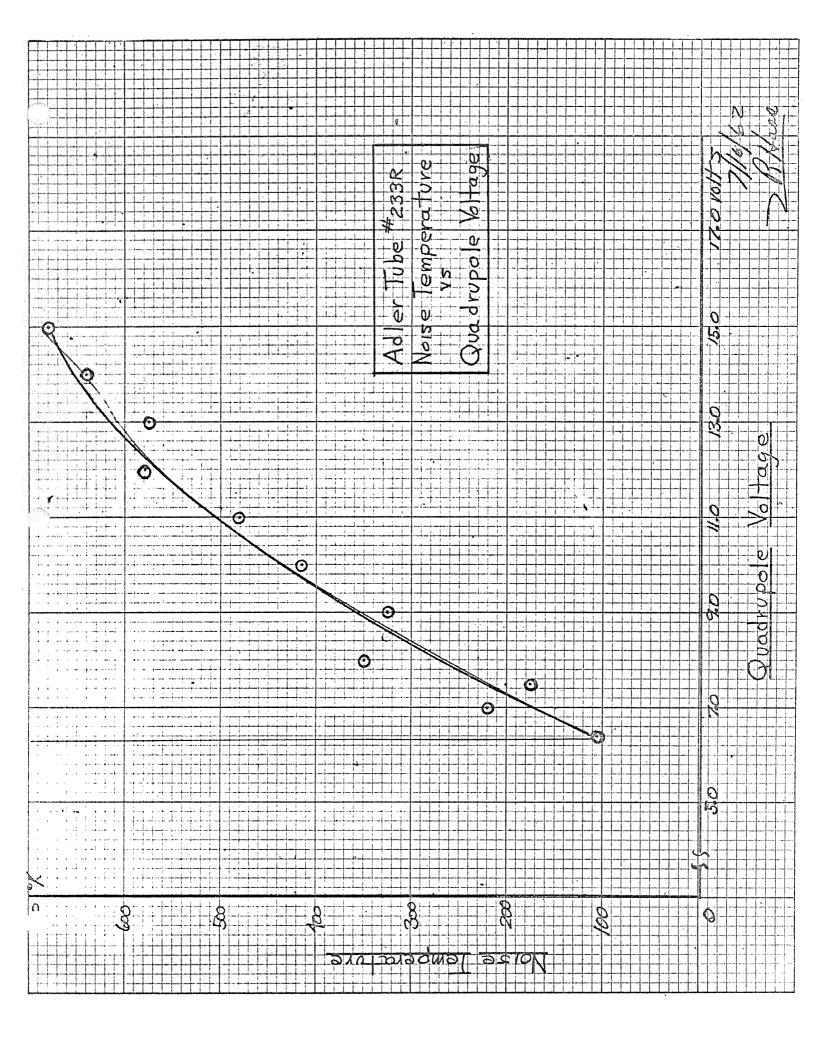


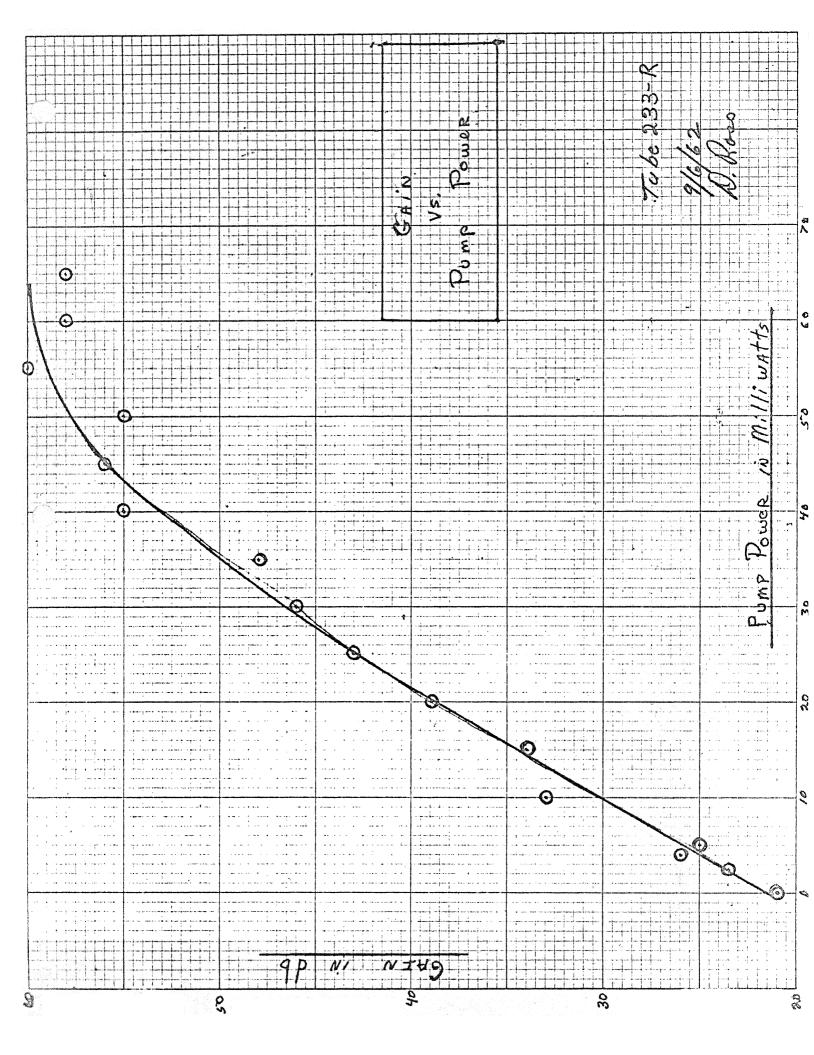


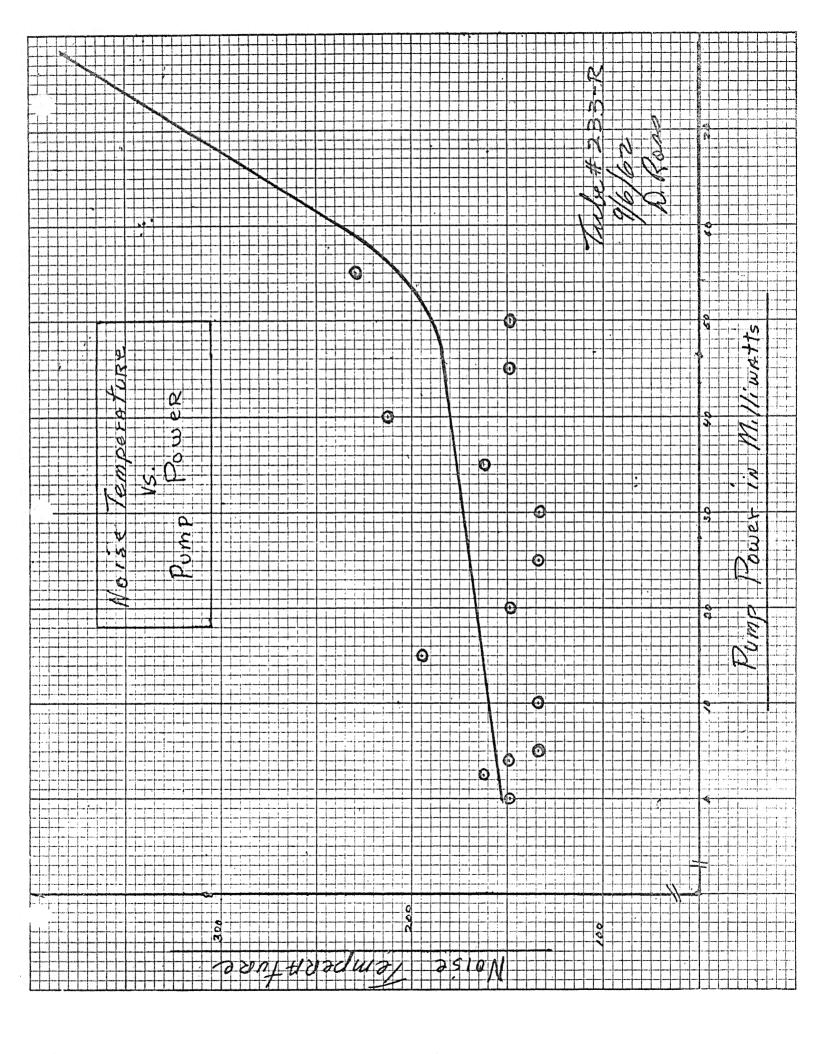












							10-3
en an de la companya		The state of the s					12/2
management in management to be a second or a second of the							
to the second of	The second secon						
and the second s							
na di Santa di Santa Santa di Santa				to the second se			
4-15-92	1100 (0)					33	
	~ j	Q	and the second s				2
And the second s	233 cto	8		The state of the s		3	
g land of the second of the se	* 8						
al dige materia consister por distributivos à servicio agricorio distributivos de la constantina del constantina del constantina de la constantina de la constantina de la constantina del constan	sen o		to colore procedure.	and a second language	B		15
	F S -	apa.		maker a second			25
	36						
\(\frac{1}{2}\)	V2 i			/	The state of the s		200
		The second secon			The state of the s	The second section is the second section of the second section of the second section of the second section section second section sect	
	*** ***********************************				The state of the s	The control of the co	- i v
or, and product relation of the continues in the continue				/ 0		e de la composition della comp	6 5
					The many terms of the control of the	y areas and a second of the second of	8
					Section of the sectio	The second secon	
The second section of the second section of the second section							2
		The second secon	to the to the second	Andreas (1997) (1994) (1995) (The second section of the section of th		
				The services of the services o			
enderenage, al. con cran majors, all assembly notes. India					• William Land green have been been been been been been been be	e mente e e e e e e e e e e e e e e e e e e	9
						Land one of the same	- 00 -
		and make the course to the	Annual to the best beautiful to the second	man an indian annan an indian y makan na kampanakan an an an an indian anan na annan anan indian an a			
0,					ten e patembrogone	7 7	0
}	K		√ 1 4	D (3 - $-$ - $-$ - $-$ - $-$ - $-$ - $-$ (6	Y
Tanàna mandra	e Mil a salah ke kua ke ke		3. · · · · · · · · · · · · · · · · · · ·				
			= sautos	adwa I	N012C	4	

