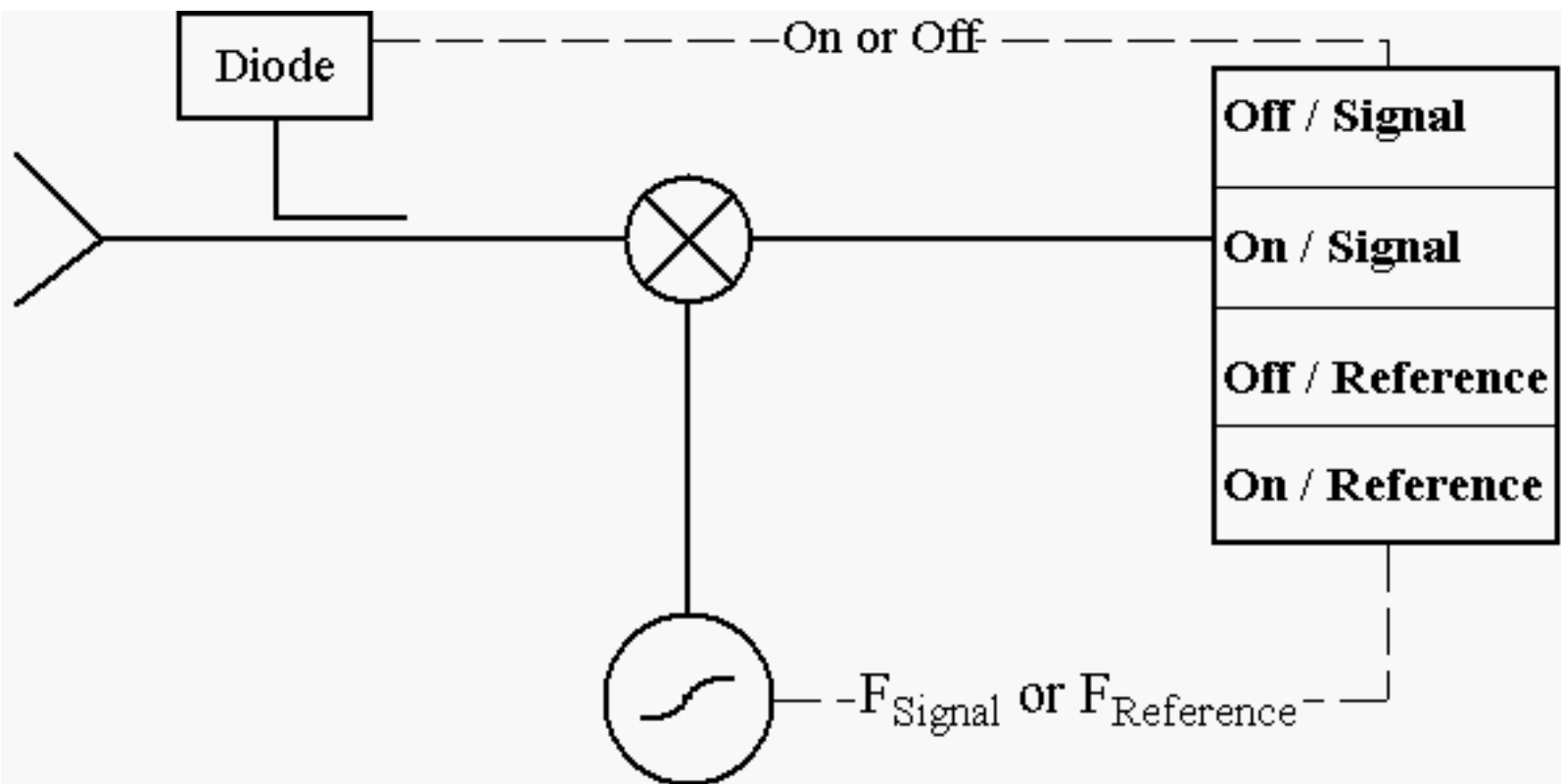




Calibration

Ron Maddalena
NRAO – Green Bank
November 2012

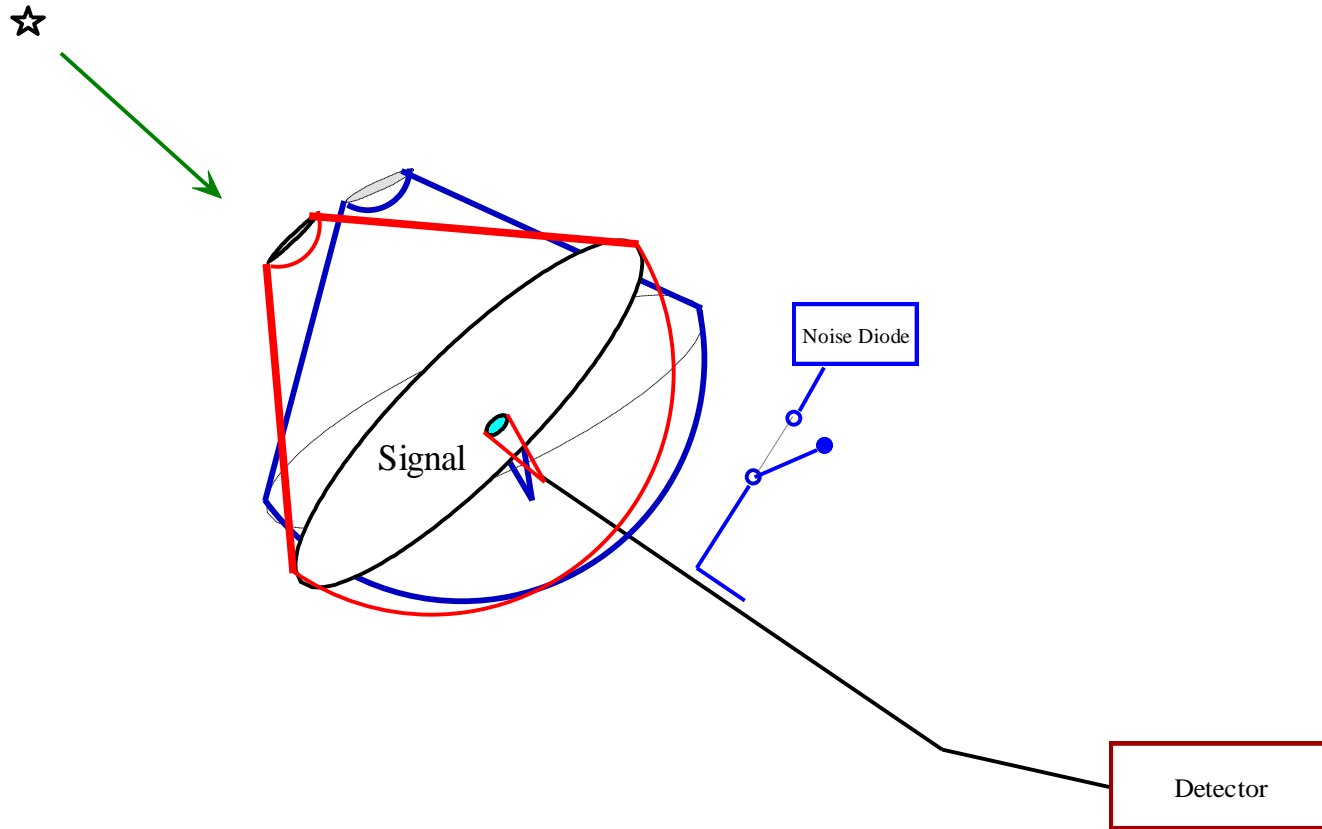


Receiver calibration sources allow us to convert the backend's detected voltages to the intensity the signal had at the point in the system where the calibration signal is injected.

Reference observations

- Difference a signal observation with a reference observation
- Types of reference observations
 - Frequency Switching
 - In or Out-of-band
 - Position Switching
 - Beam Switching
 - Move Subreflector
 - Receiver beam-switch
 - Dual-Beam Nodding
 - Move telescope
 - Move Subreflector

Position-Switched (On-Off) Observing



Typical Position-Switched Calibration Equation for a Point Source

$$S(\nu) = \left(\frac{2k}{\eta_A(\nu, Elev) \cdot Area_p} \right) \cdot T_A(\nu) \cdot e^{\tau(\nu, t) \cdot A(Elev, t)}$$

$$T_A(\nu) = \left(\frac{Sig(\nu) - Ref(\nu)}{Ref(\nu)} \right) \cdot T_{Sys}^{Ref}$$

$$T_{Sys}^{Ref} = \left\langle \frac{Ref(\nu)}{Ref_{On}(\nu) - Ref_{Off}(\nu)} T_{Cal}(\nu) \right\rangle_{BW}$$

$A(Elev, t)$ = Air Mass

$\tau(\nu, t)$ = Atmospheric Zenith Opacity

T_{cal} = Noise Diode Temperature

Area = Physical area of the telescope

$\eta_A(\nu, Elev)$ = Aperture efficiency (point sources)

$T_A(\nu)$ = Source Antenna Temperature

$S(\nu)$ = Source Flux Density

$Sig(\nu)$, $Ref(\nu)$ = Data taken on source and on blank sky (in units backend counts)

On, Off = Data taken with the noise diode on and off

T_{sys} = System Temperature averaged over bandwidth

Position-Switched Calibration Equation

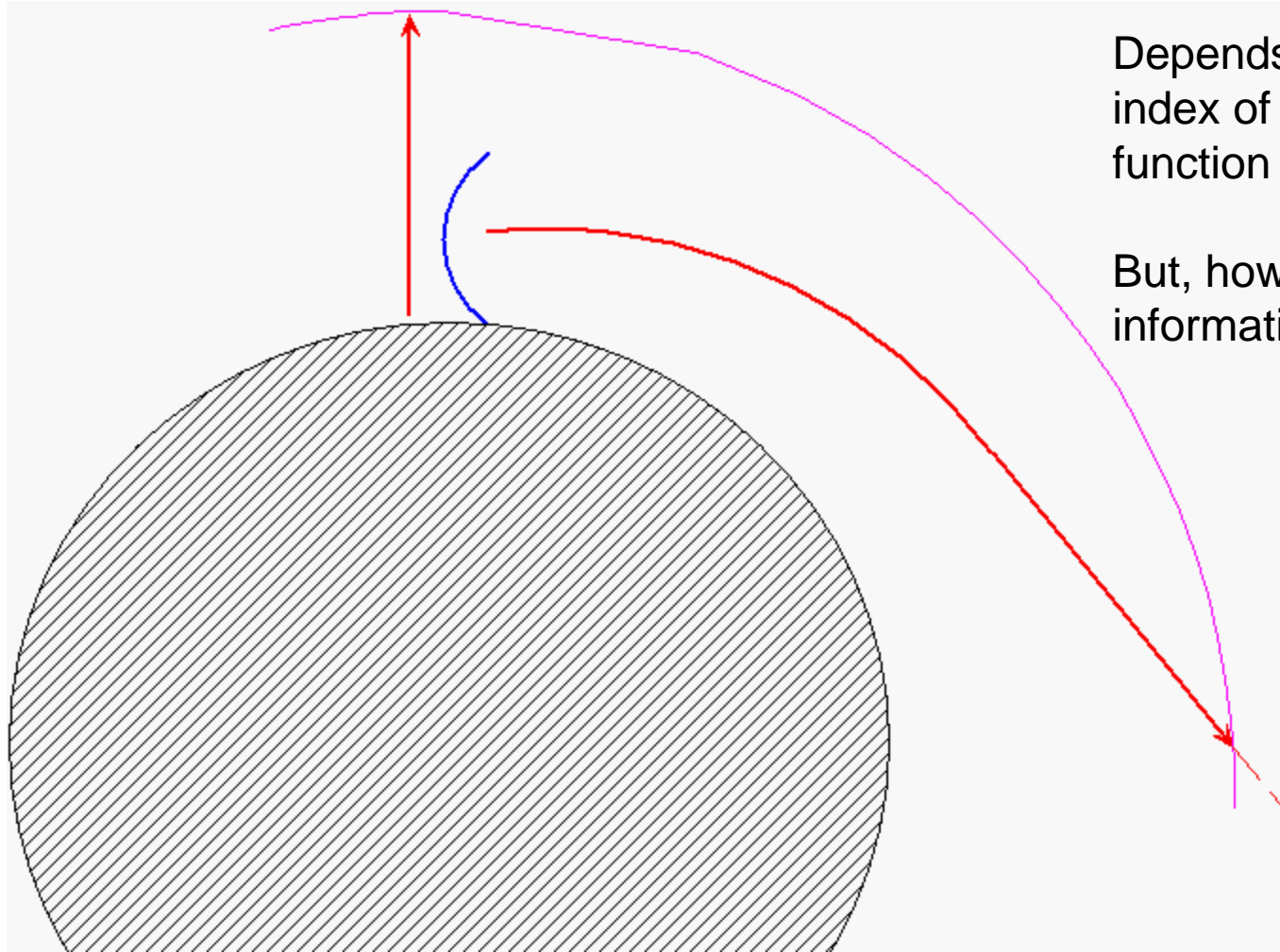
$$S(\nu) = \left(\frac{2k}{\eta_A(\nu, Elev) \cdot Area_p} \right) \cdot \left(\frac{Sig(\nu) - Ref(\nu)}{Ref(\nu)} \right) \left\langle \frac{Ref(\nu)}{Ref_{on}(\nu) - Ref_{off}(\nu)} T_{Cal}(\nu) \right\rangle \cdot e^{\tau(\nu)A(Elev)}$$

Sources of uncertainties

$$\left(\frac{\Delta S}{S} \right)^2 = (\tau \cdot \Delta A)^2 + (A \cdot \Delta \tau)^2 + \left(\frac{\Delta T_{cal}}{T_{Cal}} \right)^2 + \left(\frac{\Delta \eta}{\eta} \right)^2$$

- 10-15% accuracy have been the 'standard'
- Usually, errors in T_{cal} dominate
- Goal: To achieve 5% calibration accuracy without a significant observing overhead.

Air Mass Estimates



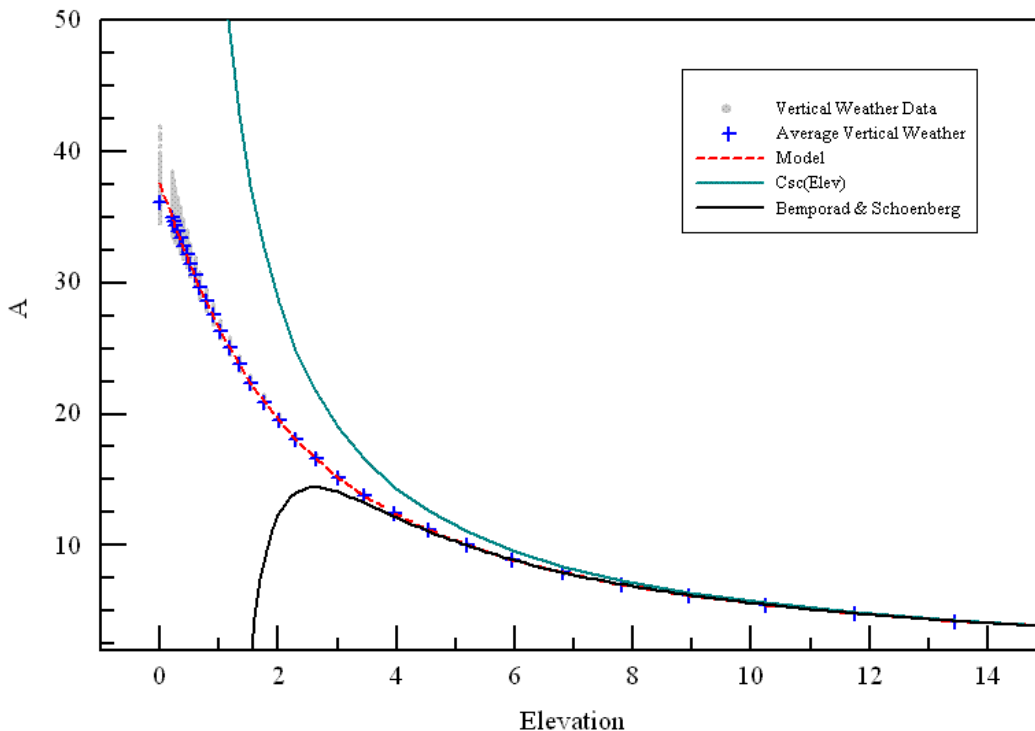
Depends upon density and index of refraction as a function of height

But, how can one get this information?

Air Mass Estimate

- Air Mass traditionally modeled as $1/\sin(\text{Elev})$
- For 1% calibration accuracy, must use a better model below 15 deg.

Air Mass



$$A = -0.0234 + \frac{1.014}{\sin\left(\text{Elev} + \frac{5.18}{\text{Elev} + 3.35}\right)}$$

- Good to 1 deg
- Use $1/\sin(\text{Elev})$ above 60 deg
- Coefficients are site specific, at some low level

Typical Position-Switched Calibration Equation

$$S(\nu) = \left(\frac{2k}{\eta_A(\nu, Elev) \cdot Area_p} \right) \cdot T_A(\nu) \cdot e^{\tau(\nu, t) \cdot A(Elev, t)}$$

$$T_A(\nu) = \left(\frac{Sig(\nu) - Ref(\nu)}{Ref(\nu)} \right) \cdot T_{Sys}^{Ref}$$

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T_{cal} = Noise Diode Temperature

Area = Physical area of the telescope

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$T_A(\nu)$ = Source Antenna Temperature

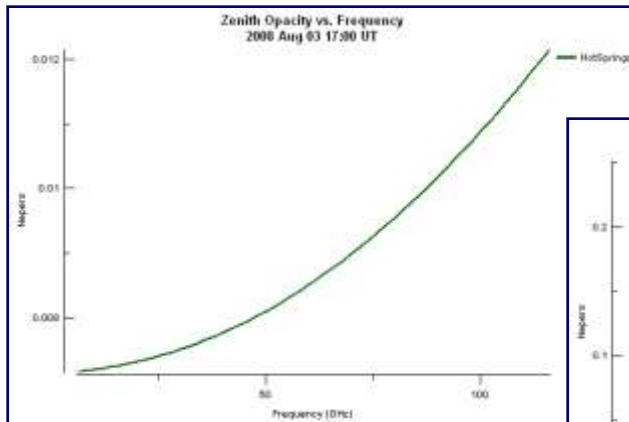
$S(\nu)$ = Source Flux Density

$Sig(\nu)$, $Ref(\nu)$ = Data taken on source and on blank sky (in units backend counts)

On, Off = Data taken with the noise diode on and off

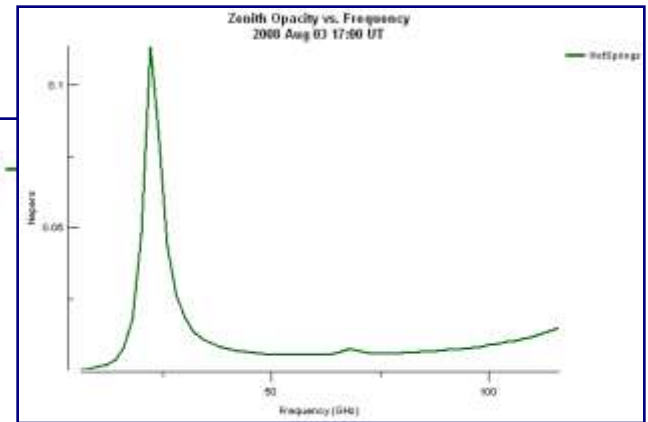
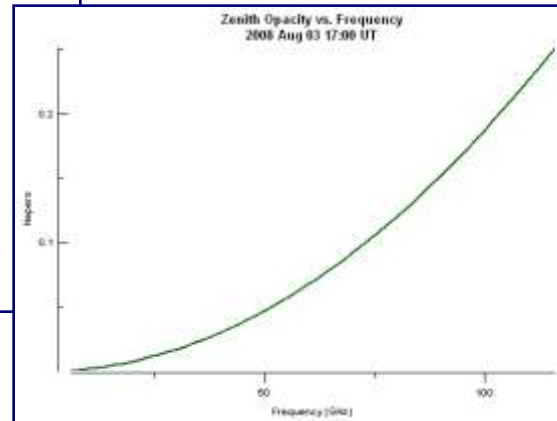
T_{sys} = System Temperature averaged over bandwidth

Opacities from the various components



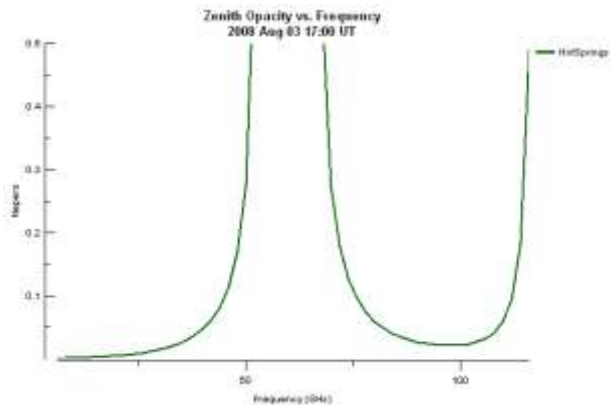
Dry Air Continuum

Water Continuum

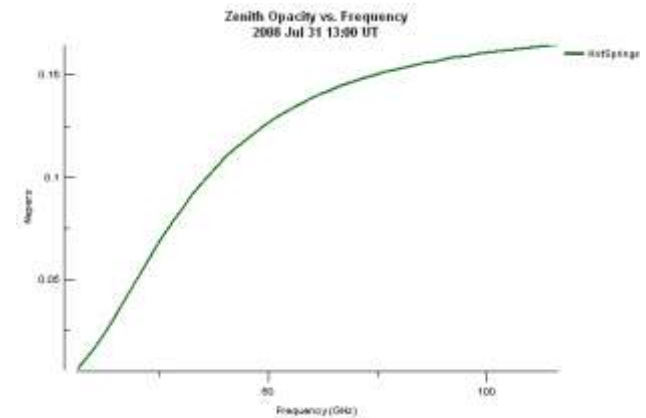


Water Line

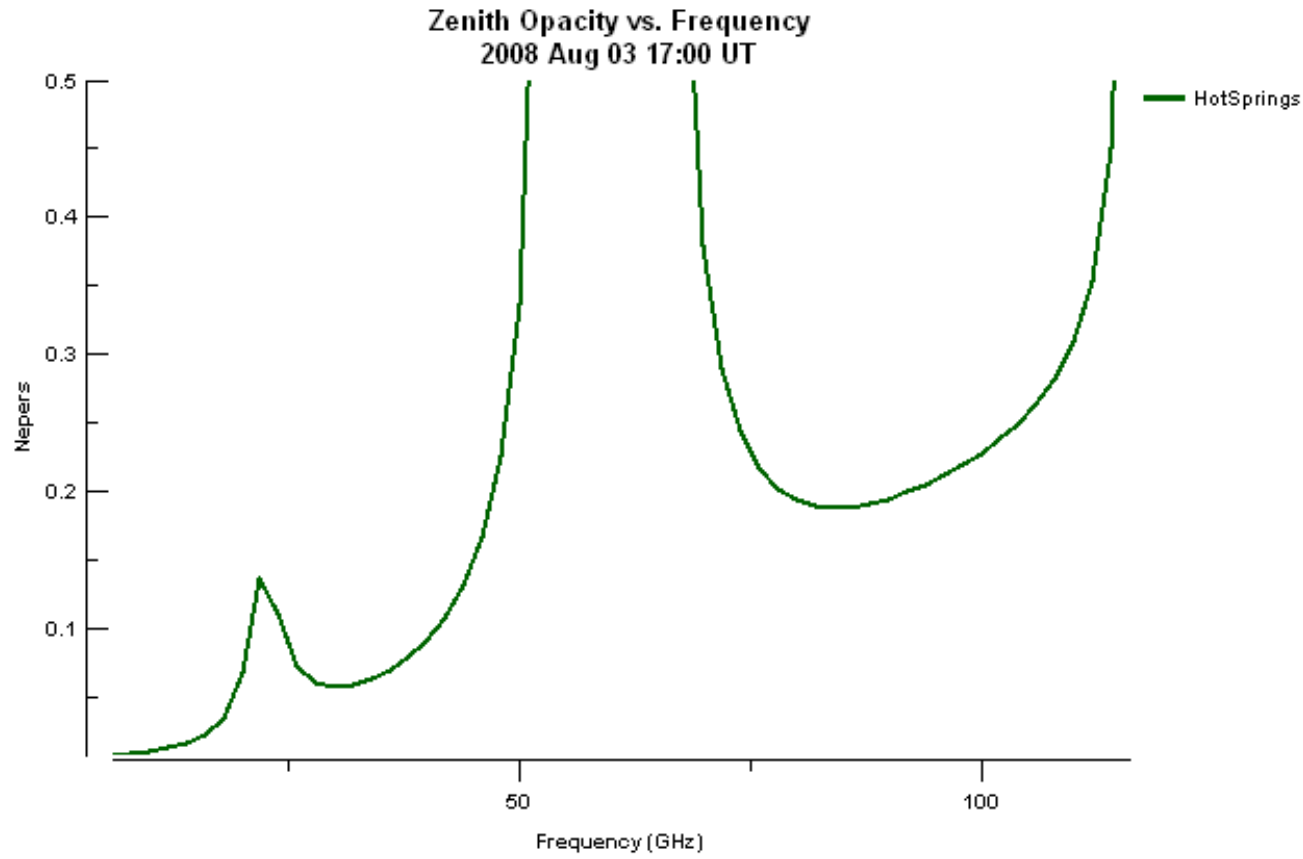
Oxygen Line



Hydrosols



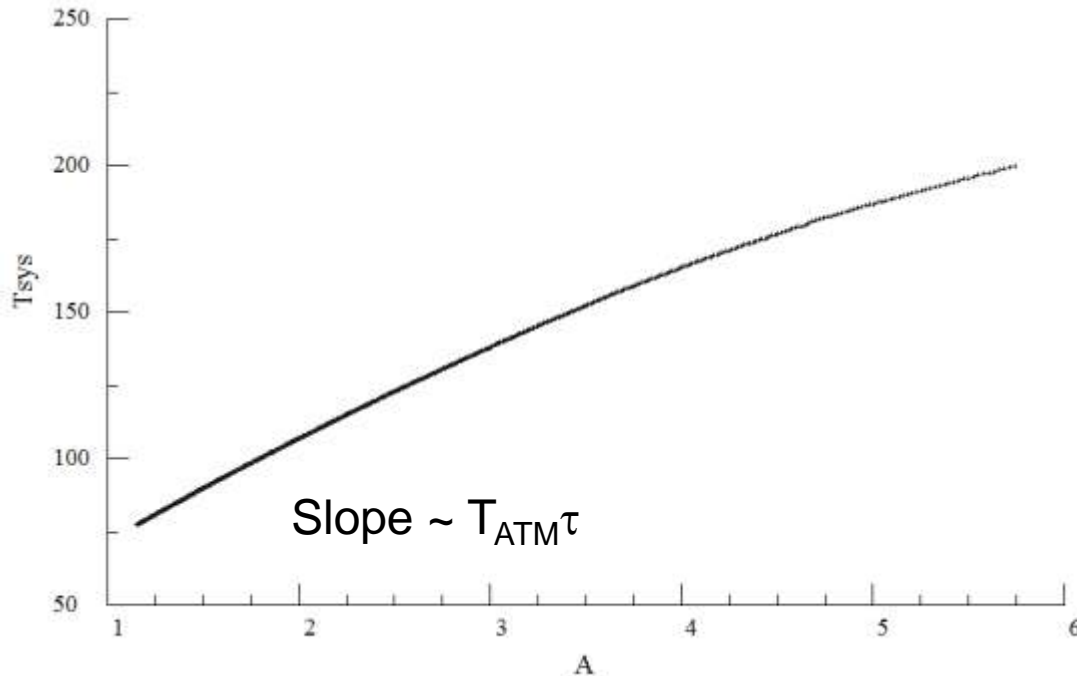
Opacities from the various components



Total Opacity

Determining Opacities

$$T_{SYS} = T_{Rcvr} + T_{Spillover} + T_{CMB}e^{-\tau \cdot A} + T_{ATM} \cdot (1 - e^{-\tau \cdot A})$$



Typical Position-Switched Calibration Equation

$$S(\nu) = \left(\frac{2k}{\eta_A(\nu, Elev) \cdot Area_p} \right) \cdot T_A(\nu) \cdot e^{\tau(\nu, t) \cdot A(Elev, t)}$$

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$S(\nu)$ = Source Flux Density

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On, Off = Data taken with the noise diode on and off

T_{sys} = System Temperature averaged over bandwidth

Determining T_{Cal} from hot-cold load measurements in the lab

- Place black bodies (absorbers) of two known temperatures in front of the feed and record detected voltages.
 - $V_{Hot_Off} = g * T_{Hot}$
 - $V_{Cold_Off} = g * T_{Cold}$
 - $V_{Cold_On} = g * (T_{Cold} + T_{Cal})$
- g and T_{Cal} are unknown

Determining T_{Cal} from hot-cold load measurements in the lab

$$T_{\text{Cal}} = \frac{V_{\text{Cold_On}} - V_{\text{Cold_Off}}}{V_{\text{Hot_Off}} - V_{\text{Cold_Off}}} \cdot (T_{\text{Hot}} - T_{\text{Cold}})$$

- Course frequency resolution
- Uncertainties in load temperatures
- Are the absorbers black bodies?
- Detector linearities (300 & 75 K)
- Lab T_{Cal} may be off by 10%
- So... all good observers perform their own astronomical calibration observation

Noise Diode Estimates

- Instead, we recommend an On-Off observation
 - Use a point source with known flux -- polarization should be low or understood
 - Use the same exact hardware, exact setup as your observation. (i.e., don't use your continuum pointing data to calibrate your line observations.)
 - Observations take ~5 minutes per observing run
 - Staff take about 2 hrs to measure the complete band of a high-frequency, multi-beam receiver.
 - Resolution sufficient: 1 MHz, sometimes better
 - Accuracy of ~ 1%, mostly systematics.

Noise Diode Estimates

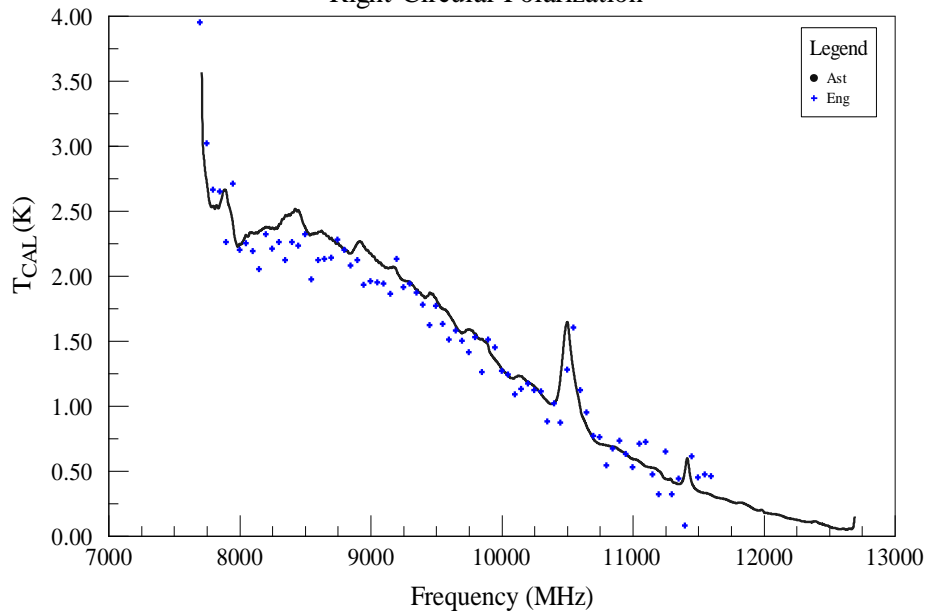
$$S(\nu) = \left(\frac{2k}{\eta_A(\nu, Elev) \cdot A_p} \right) \cdot \left(\frac{Sig(\nu) - Ref(\nu)}{Ref(\nu)} \right) \left\langle \frac{Ref(\nu)}{Ref_{on}(\nu) - Ref_{off}(\nu)} T_{Cal}(\nu) \right\rangle \cdot e^{\tau(\nu)A}$$

Remove Averaging, Solve for Tcal

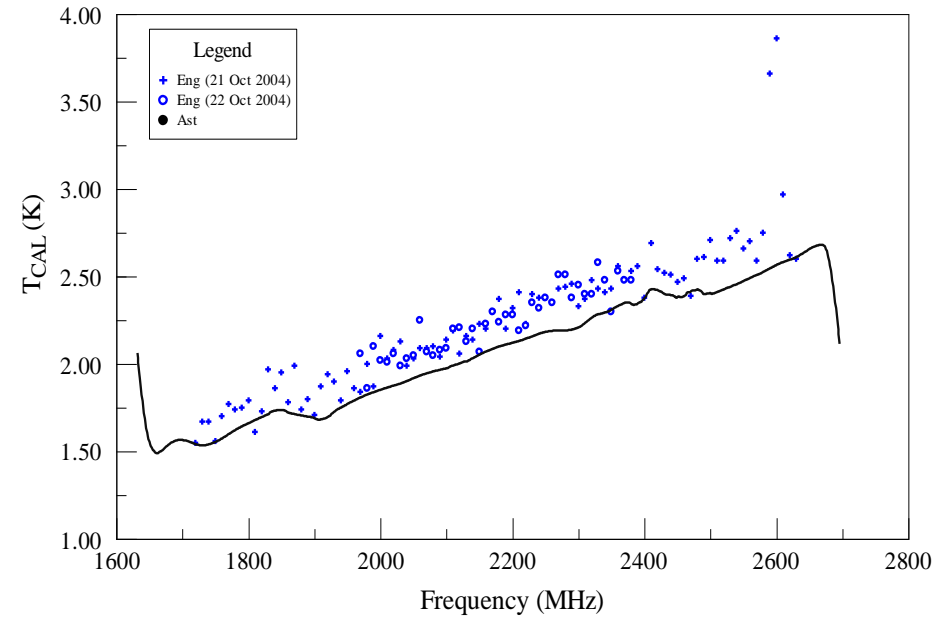
$$T_{Cal}(\nu) = \frac{\eta_A(\nu, Elev) \cdot Area_p}{2k \cdot e^{\tau(\nu) \cdot A}} \left(\frac{Ref_{on}(\nu) - Ref_{off}(\nu)}{Sig(\nu) - Ref(\nu)} \right) \cdot S(\nu)$$

Noise Diode Estimates

X-band Low Cals
Right-Circular Polarization



S-band Low Cals
Y-Linear Polarization



Typical Position-Switched Calibration Equation

$$S(\nu) = \left(\frac{2k}{\eta_A(\nu, Elev) \cdot Area_p} \right) \cdot T_A(\nu) \cdot e^{\tau(\nu, t) \cdot A(Elev, t)}$$

$$T_A(\nu) = \left(\frac{Sig(\nu) - Ref(\nu)}{Ref(\nu)} \right) \cdot T_{Sys}^{Ref}$$

$$T_{Sys}^{Ref} = \left\langle \frac{Ref(\nu)}{Ref_{On}(\nu) - Ref_{Off}(\nu)} T_{Cal}(\nu) \right\rangle_{BW}$$

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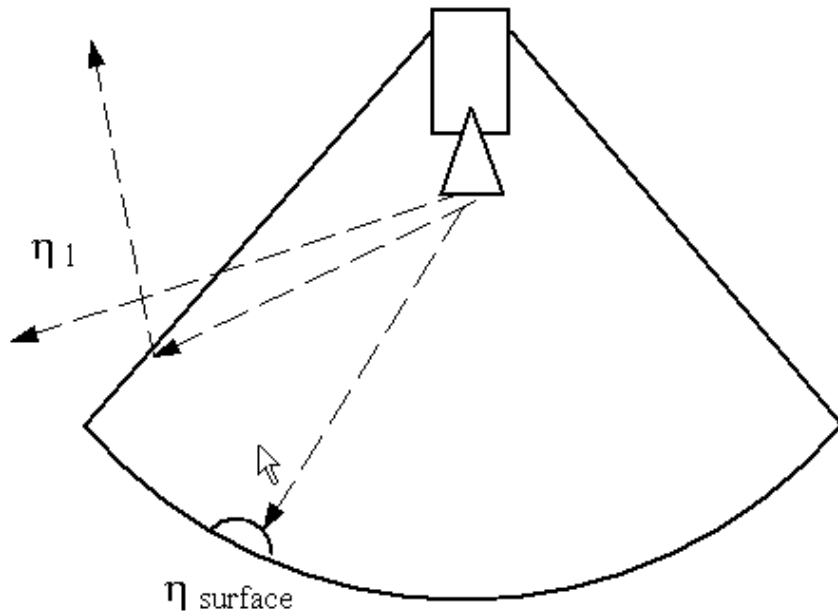
$S(\nu)$ = Source Flux Density

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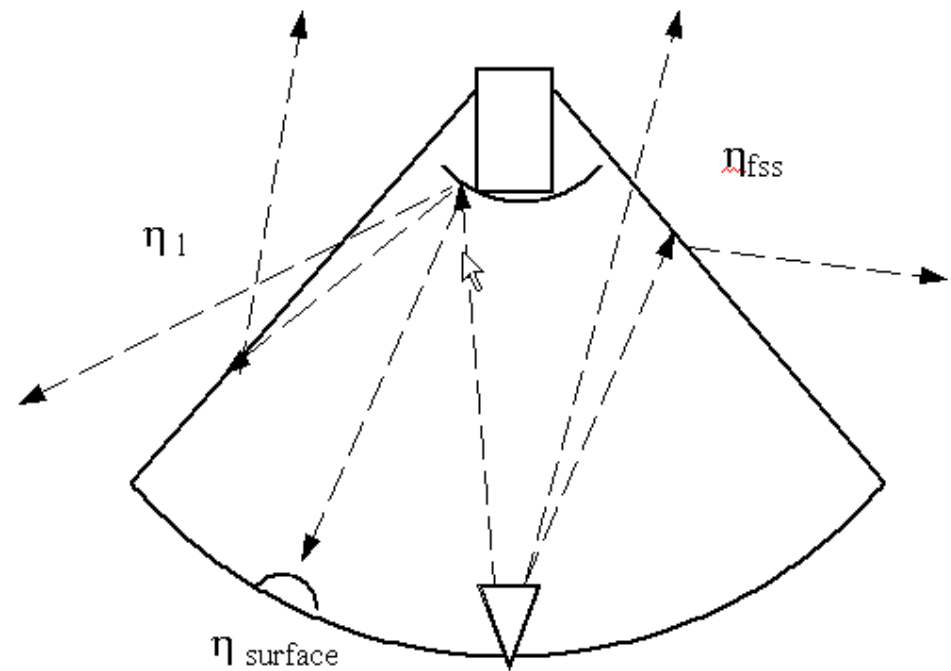
On, Off = Data taken with the noise diode on and off

T_{sys} = System Temperature averaged over bandwidth

Telescope efficiencies – Part 1



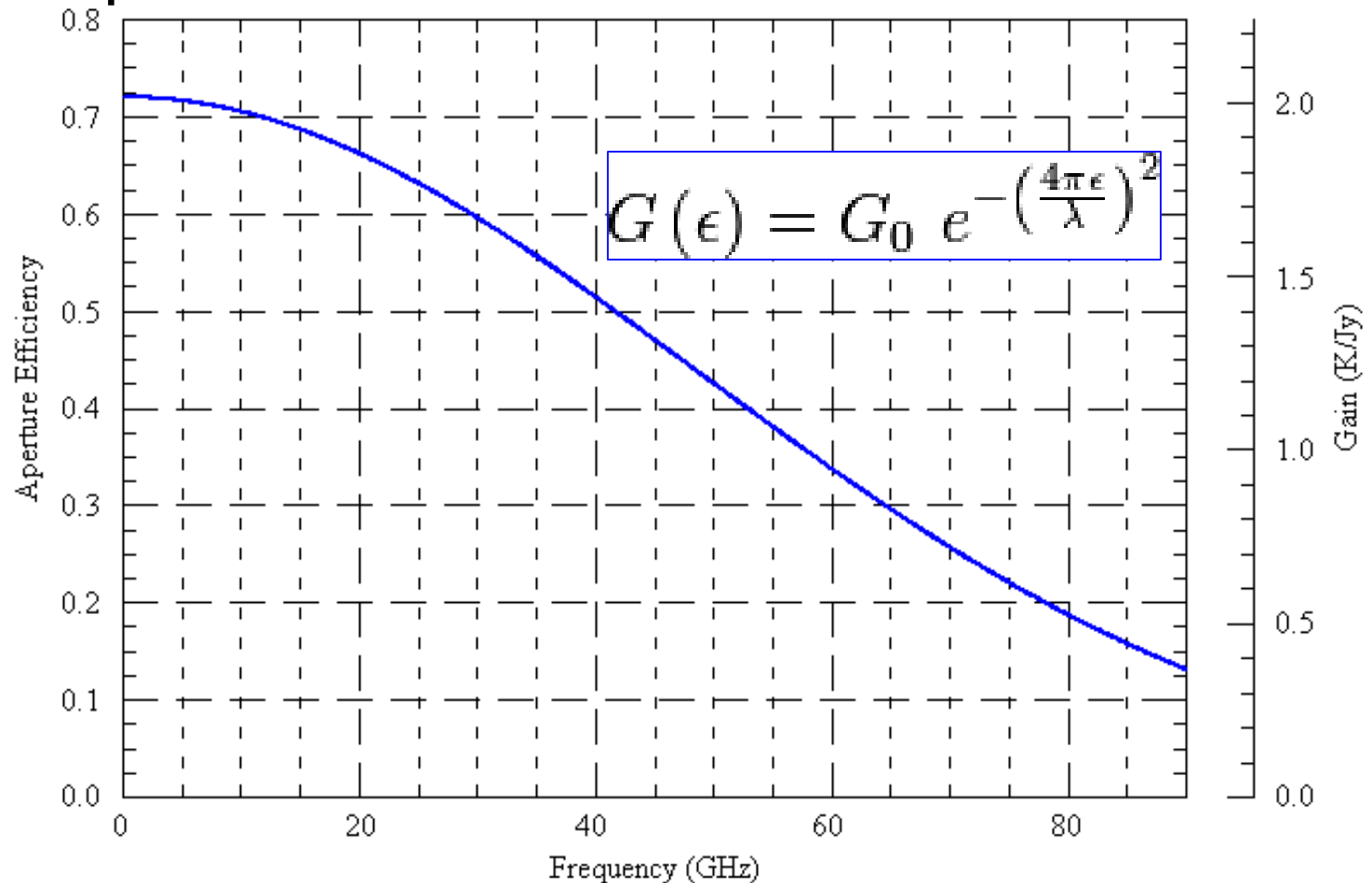
Not shown: η_r and $\eta_{\text{illumination}}$



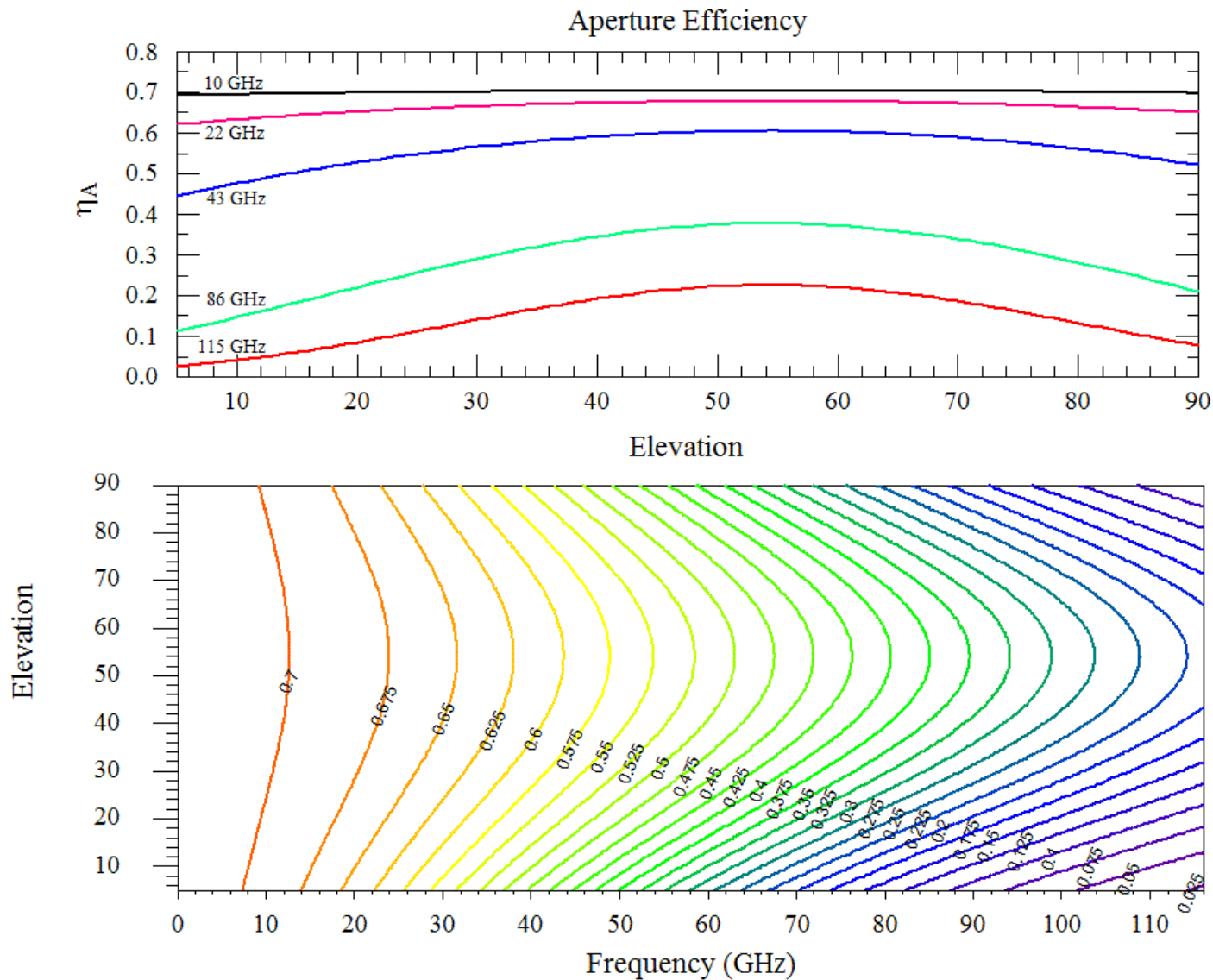
Not shown: η_r and $\eta_{\text{illumination}}$

GBT Gain Curve

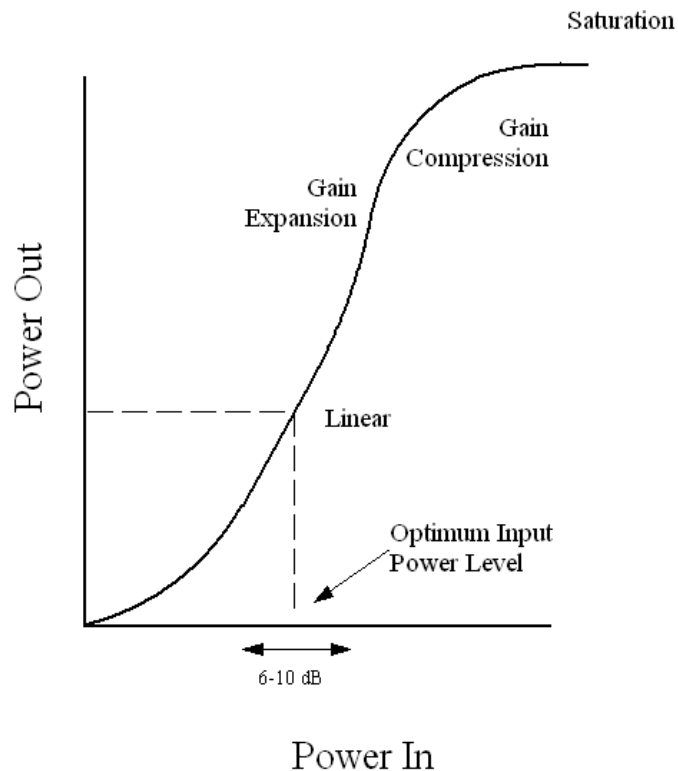
Ruze Equation – Surface errors



GBT Gain Curve

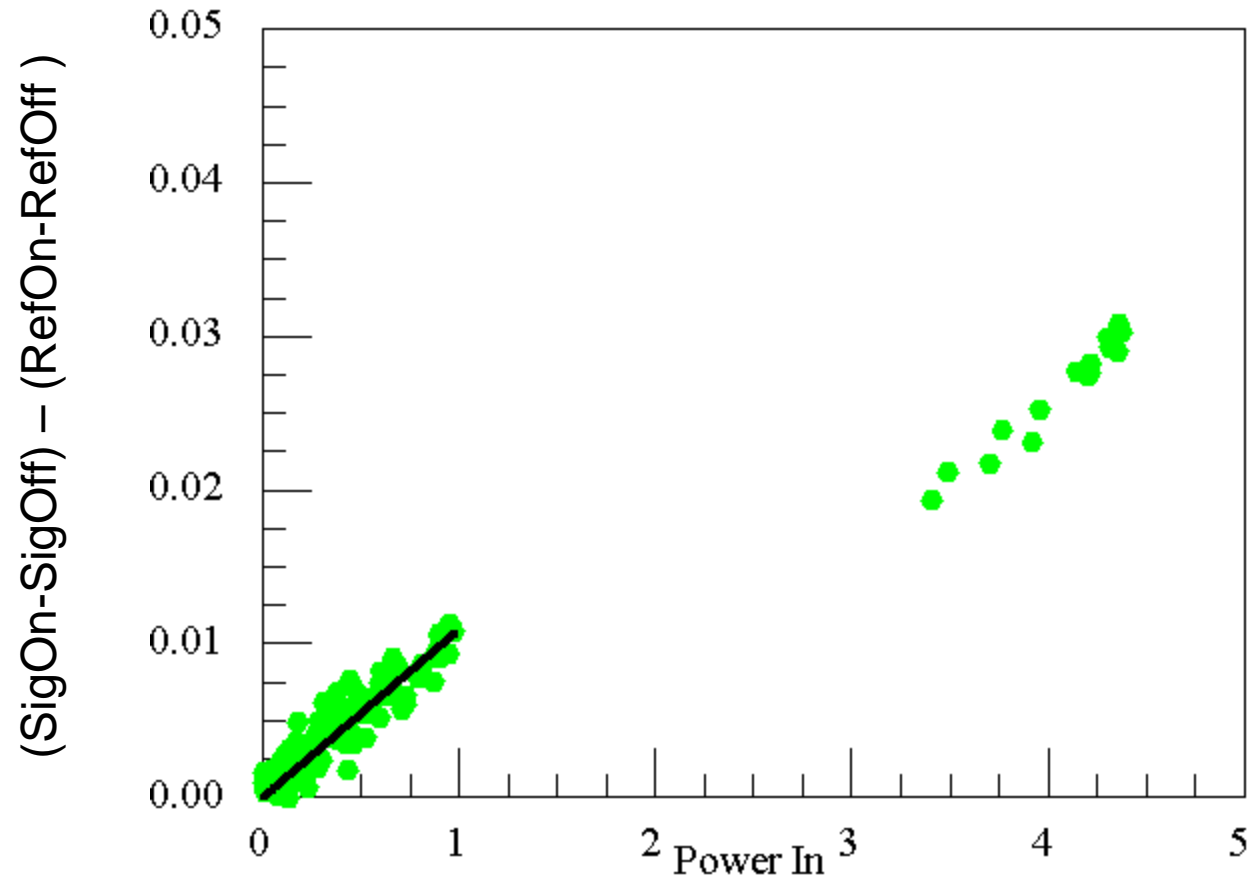


Non-linearity



- If system is linear,
 - $P_{out} = B * P_{in}$
 - $(Sig_{on} - Sig_{off}) - (Ref_{on} - Ref_{off}) = 0$
- Model the response curve to 2nd order:
 - $P_{out} = B * P_{in} + C * P_{in}^2$
- Our 'On-Off' observations of a calibrator provide:
 - Four measured quantities: Ref_{off} , Ref_{on} , Sig_{off} , Sig_{on}
 - T_A From catalog
 - Four desired quantities: B , C , T_{cal} , T_{sys}
- It's easy to show that:
 - $C = [(Sig_{on} - Sig_{off}) - (Ref_{on} - Ref_{off})] / (2T_A T_{cal})$
- Thus:
 - Can determine if system is sufficiently linear
 - Can correct to 2nd order if it is not

Non-linearity



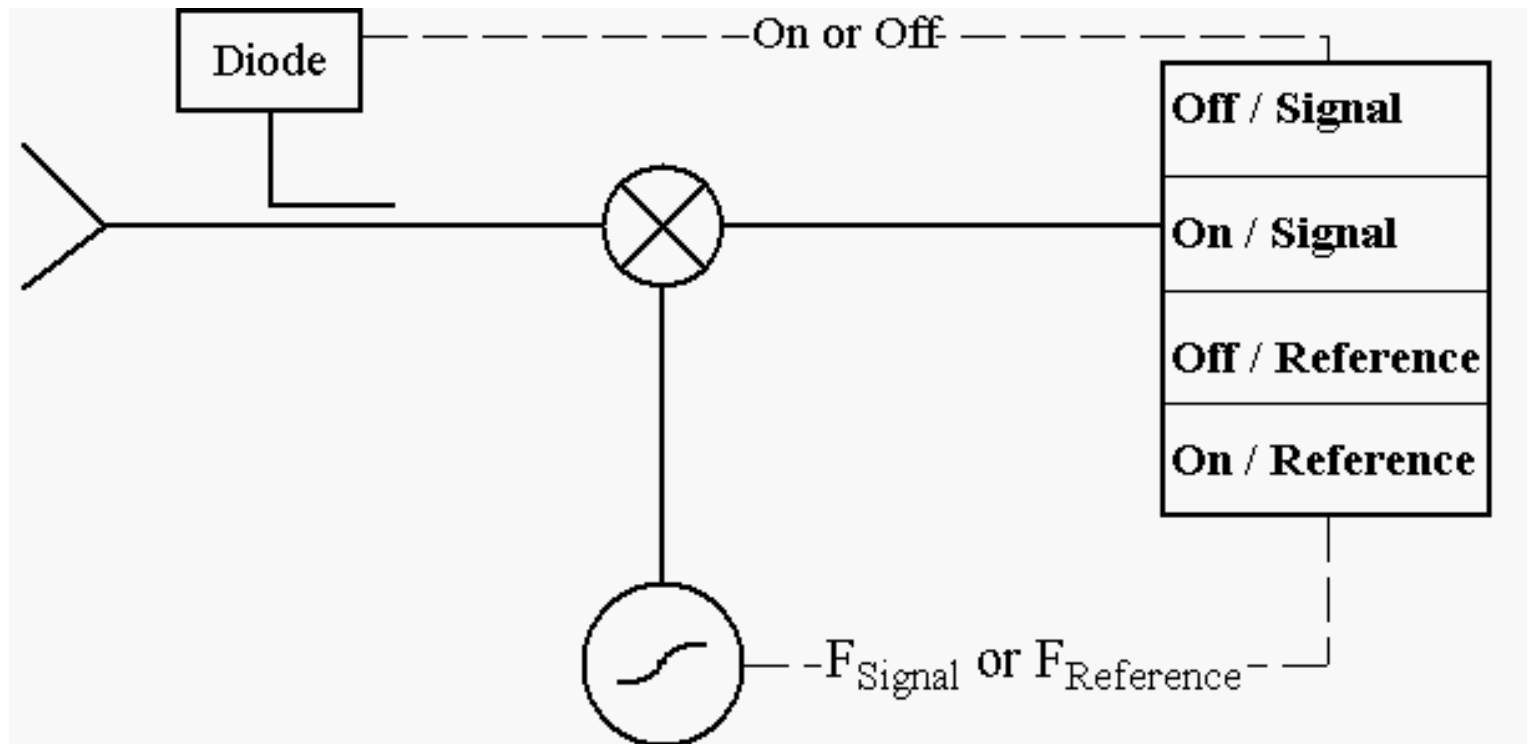
Reference observations

- Difference a signal observation with a reference observation
- Types of reference observations
 - Frequency Switching
 - In or Out-of-band
 - Position Switching
 - Beam Switching
 - Move Subreflector
 - Receiver beam-switch
 - Dual-Beam Nodding
 - Move telescope
 - Move Subreflector

Position switching

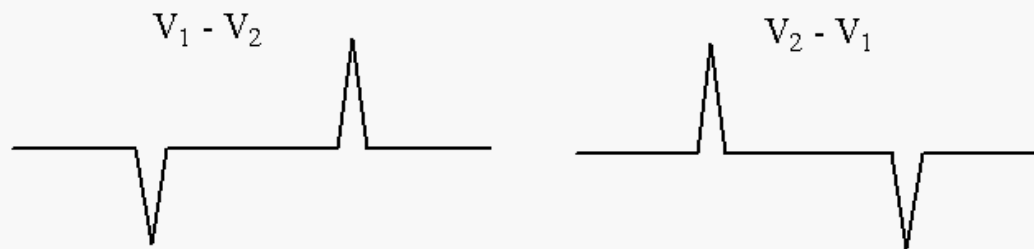
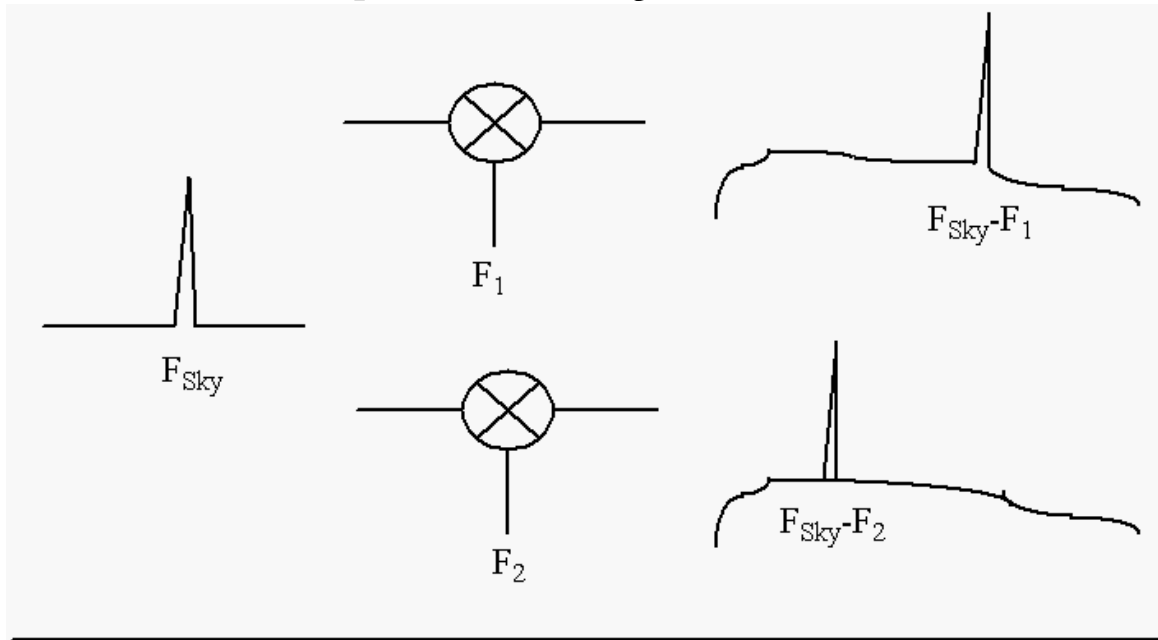
- Move the telescope between a signal and reference position
 - Overhead
 - $\frac{1}{2}$ time spent off source
- Difference the two spectra
- Assumes shape of gain/bandpass doesn't change between the two observations.
- For strong sources, must contend with dynamic range and linearity restrictions.

Frequency switching



- Eliminates bandpass shape from components after the mixer
- Leaves the derivative of the bandpass shape from components before the mixer.

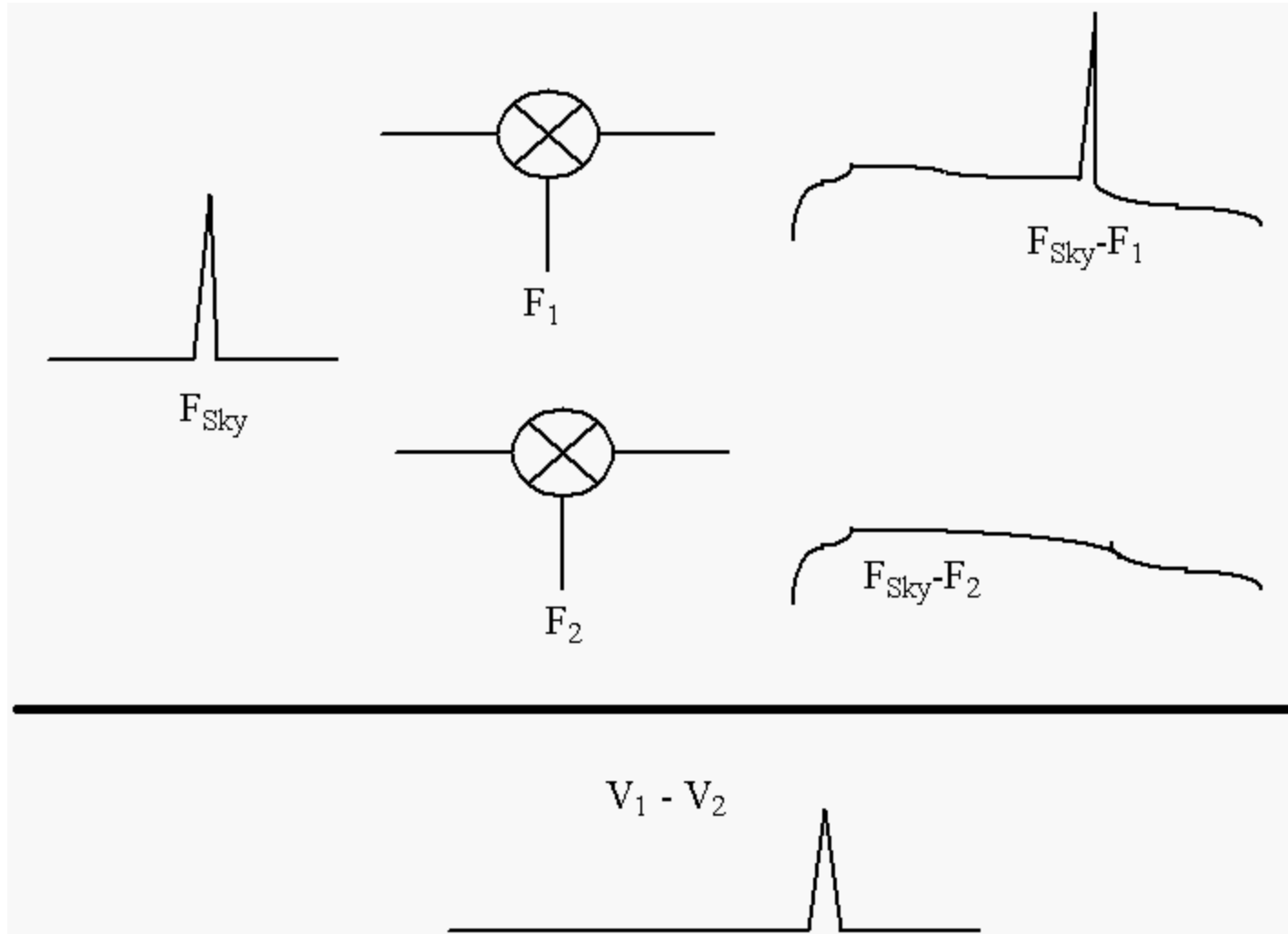
In-Band Frequency Switching



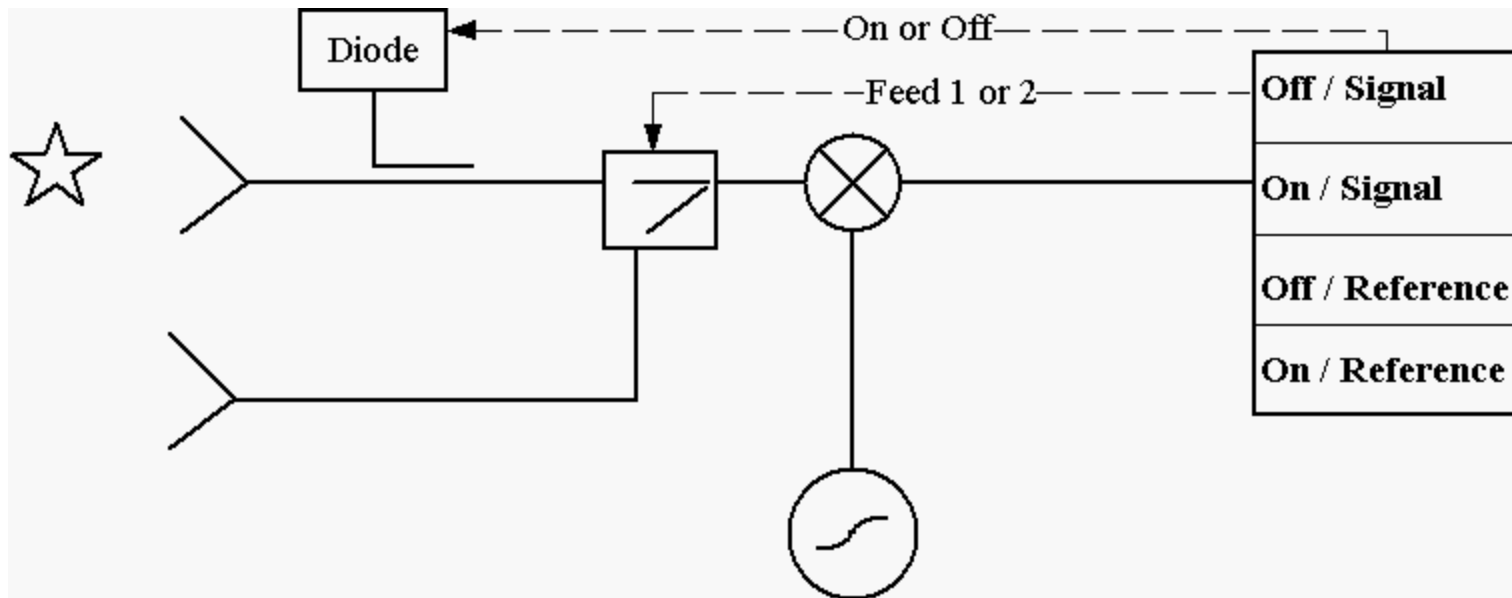
Shift and Average to decrease noise by $\sqrt{2}$



Out-Of-Band Frequency Switching



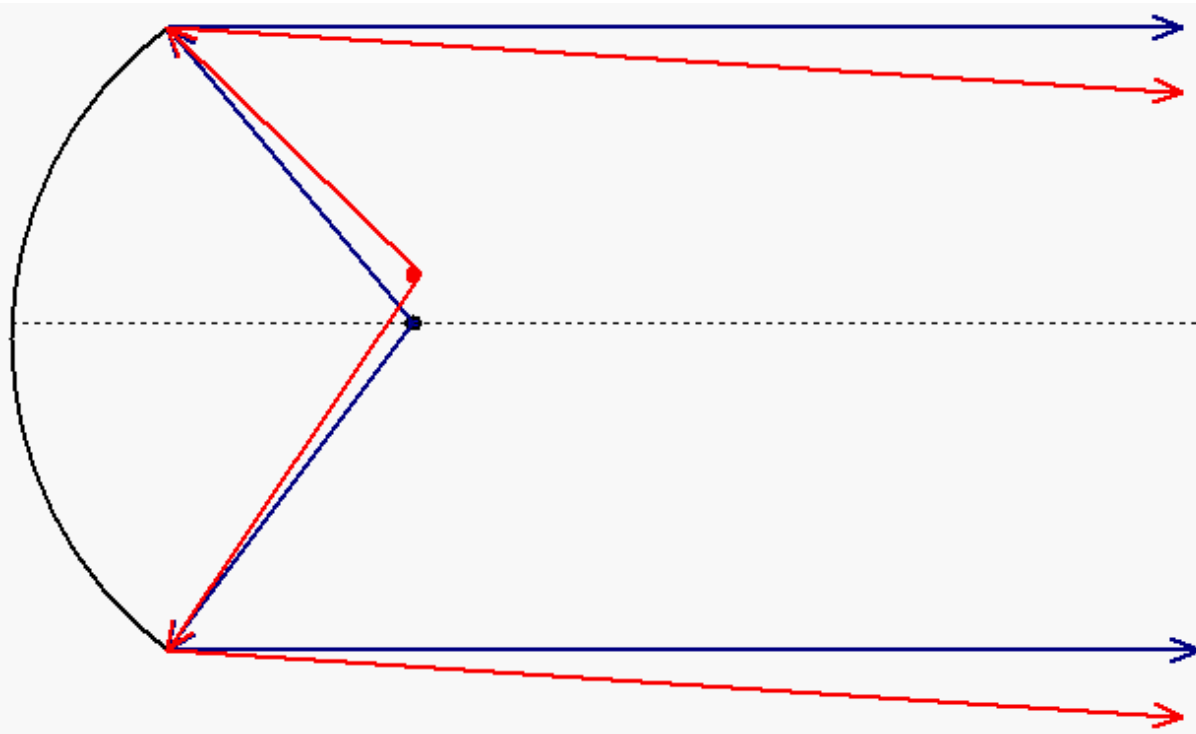
Beam switching – Internal switch



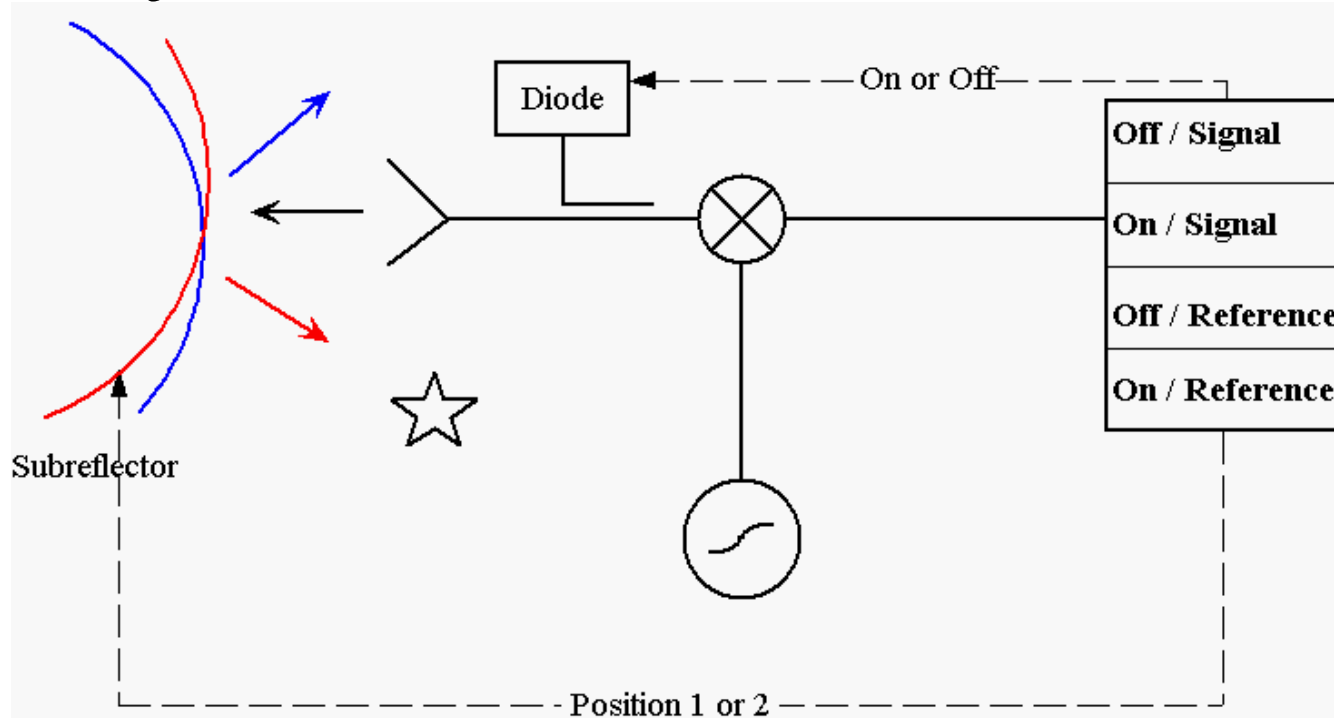
- Difference spectra eliminates any contributions to the bandpass from after the switch
- Residual will be the difference in bandpass shapes from all hardware in front of the switch.
- Low overhead but $\frac{1}{2}$ time spent off source

Atmosphere is in the near field

- Common to all feeds in a multi-feed receiver

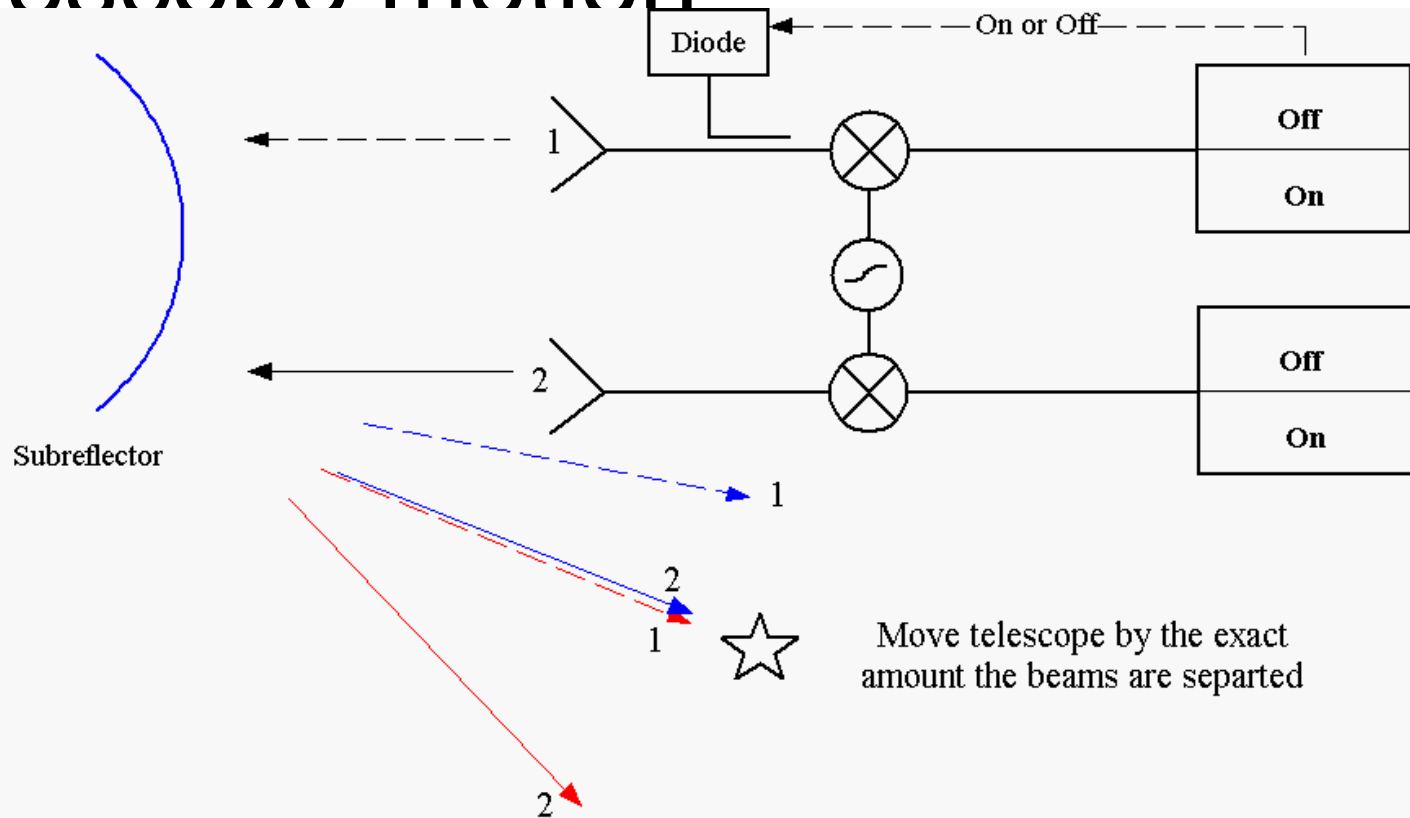


Beam Switching – Subreflector or tertiary mirror



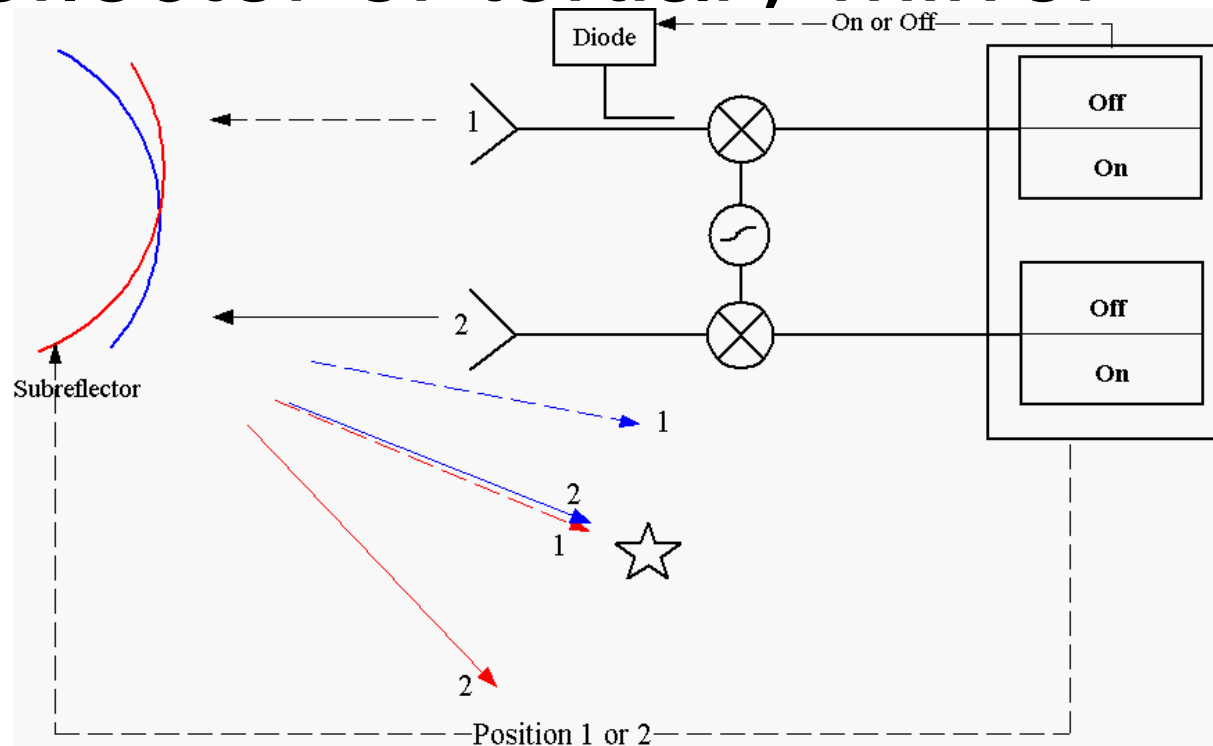
- Optical aberrations
- Difference in spillover/ground pickup
- Removes any 'fast' gain/bandpass changes
- Low overhead. $\frac{1}{2}$ time spent off source

Nodding with dual-beam receivers - Telescope motion



- Optical aberrations
- Difference in spillover/ground pickup
- Removes any 'fast' gain/bandpass changes
- Overhead from moving the telescope. All the time is spent on source

Nodding with dual-beam receivers - Subreflector or tertiary mirror



- Optical aberrations
- Difference in spillover/ground pickup
- Removes any 'fast' gain/bandpass changes
- Low overhead. All the time is spent on source

References

- Rohlfs & Wilson, “Tools of Radio Astronomy”
- Stanimirovic et al, “Single-Dish Radio Astronomy: Techniques and Practices”
- Baars, 1973, IEEE Trans Antennas Propagat, Vol AP-21, no. 4, pp 461-474
- Kutner & Ulich, 1981, Astronomica Journal, Vol 250,pp 341-348
- Winkel, Kraus, & Bach, 2012, Astronomy & Astrophysics, vol. 540.