

**NATIONAL RADIO ASTRONOMY OBSERVATORY  
Charlottesville, VA**

**ELECTRONICS DIVISION TECHNICAL NOTE NO. 215**

**Mismatch Caused by Waveguide Tolerances,  
Corner Radii, and Flange Misalignment**

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## Mismatch Caused by Waveguide Tolerances, Corner Radii, and Flange Misalignment

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The results given below were obtained using the EM simulator QuickWave. Approximate analytical formulas for the reflection coefficients of junctions of waveguides with slightly different dimensions are given by Banister *et al.* [1]. A formula for the effect of finite corner radii on cutoff frequency is given by Brady [2].

### Effect of $a$ - and $b$ -dimension tolerances

Figs. 1 and 2 show the reflection coefficient of a mated pair of waveguides with 2:1 nominal aspect ratio whose  $a$  and  $b$  dimensions include the maximum allowed tolerances. As in the MIL-DTL-85/3C standard, it is assumed that  $a$  and  $b$  are specified with the same tolerance,  $\pm t$ . In Fig. 1, one waveguide has the maximum possible width ( $a + t$ ) and minimum height ( $b - t$ ), and the other has minimum width ( $a - t$ ) and maximum height ( $b + t$ ). In Fig. 2, one waveguide has the maximum possible width ( $a + t$ ) and height ( $b + t$ ), and the other minimum width ( $a - t$ ) and height ( $b - t$ ). It is clear that the configuration in Fig. 1 produces a larger reflection than that in Fig. 2, and Fig. 1 should therefore be used as a basis for setting the tolerance on waveguide dimensions.

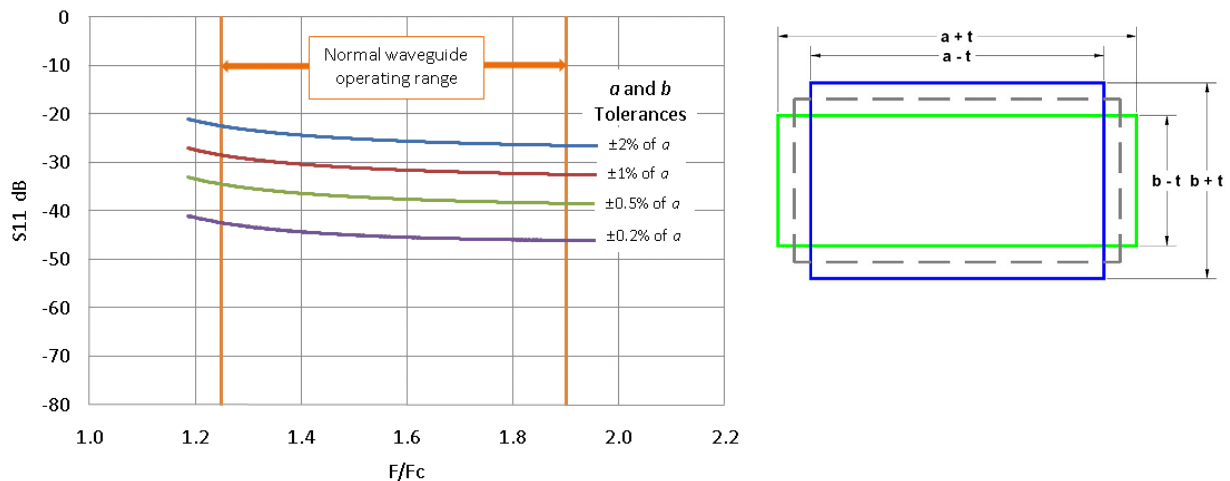


Fig. 1. Reflection coefficient of a junction of two rectangular waveguides with 2:1 nominal aspect ratio. Waveguide 1:  $(a - t) \times (b + t)$ . Waveguide 2:  $(a + t) \times (b - t)$ .  $t$  is the tolerance on both  $a$  and  $b$ .

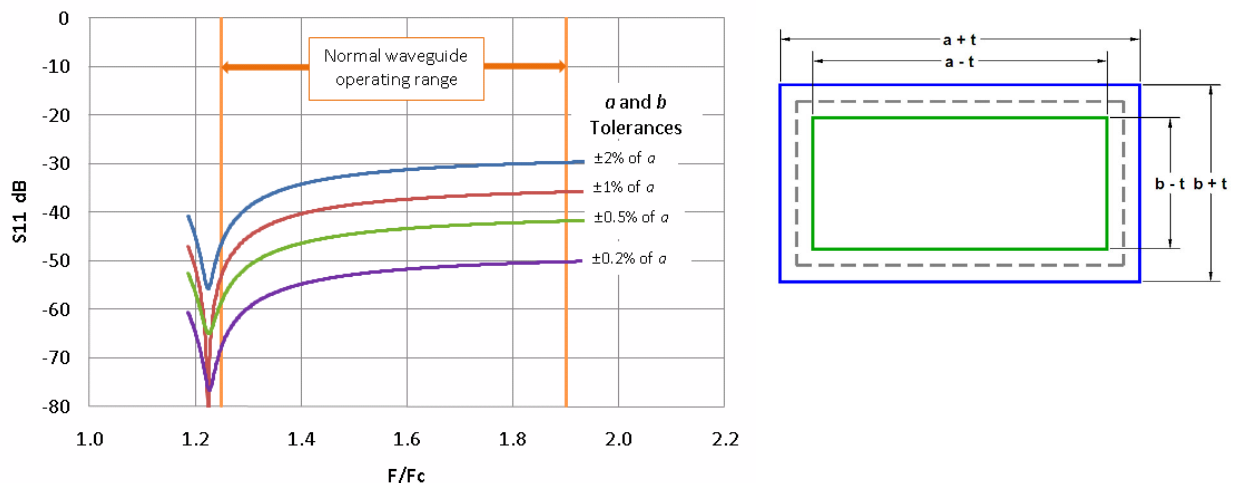


Fig. 2. Reflection coefficient of a junction of two rectangular waveguides with 2:1 nominal aspect ratio. Waveguide 1:  $(a + t) \times (b + t)$ . Waveguide 2:  $(a - t) \times (b - t)$ .  $t$  is the tolerance on both  $a$  and  $b$ .

### Effect of corner radii

Fig. 3 shows the reflection coefficient of a waveguide with 2:1 aspect ratio and finite corner radii ( $R$ ) connected to a perfectly rectangular waveguide with the same height ( $b$ ) and width ( $a$ ). The solid curves are the results of an EM simulation of this configuration. According to Brady [2], a rectangular waveguide with small corner radii is equivalent to a perfectly rectangular waveguide with the same height  $b$  and the width  $a$  adjusted to give the same aperture area. The dashed curves in Fig.3 (barely visible on top of the solid curves) are for a junction of two perfectly rectangular waveguides, one of whose width is adjusted using Brady's rule to correspond to the given corner radius.

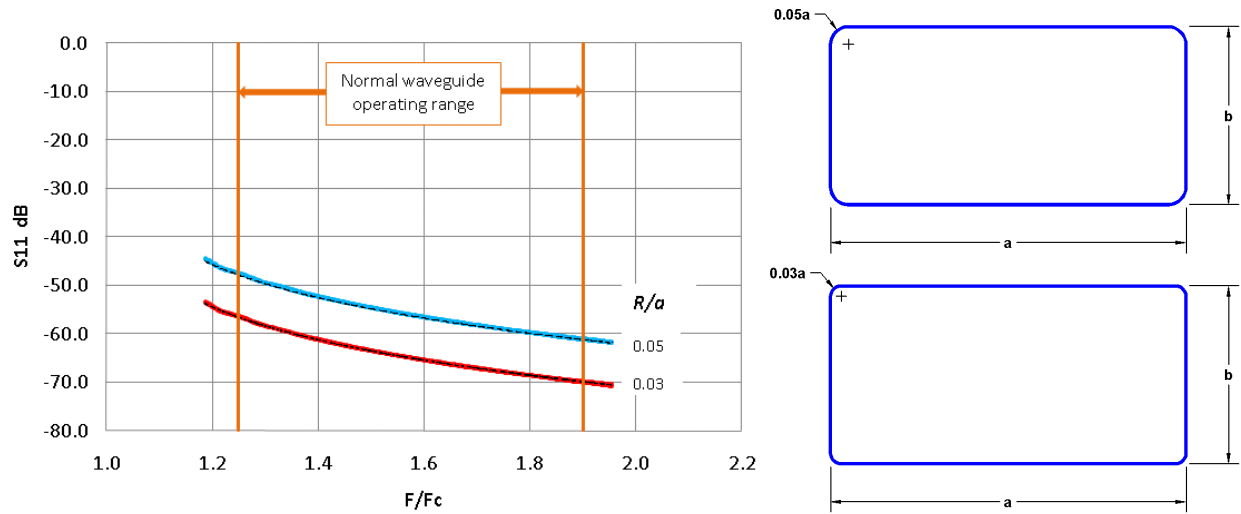


Fig. 3. Reflection coefficient of a perfectly rectangular waveguide of 2:1 aspect ratio connected to one of the same dimensions but with corner radii  $R$ .

### Effect of linear flange misalignment

Figs. 4 and 5 show the reflection coefficient of a junction of two rectangular waveguides with 2:1 aspect ratio, misaligned in the  $a$ -direction and in the  $b$ -direction, respectively.

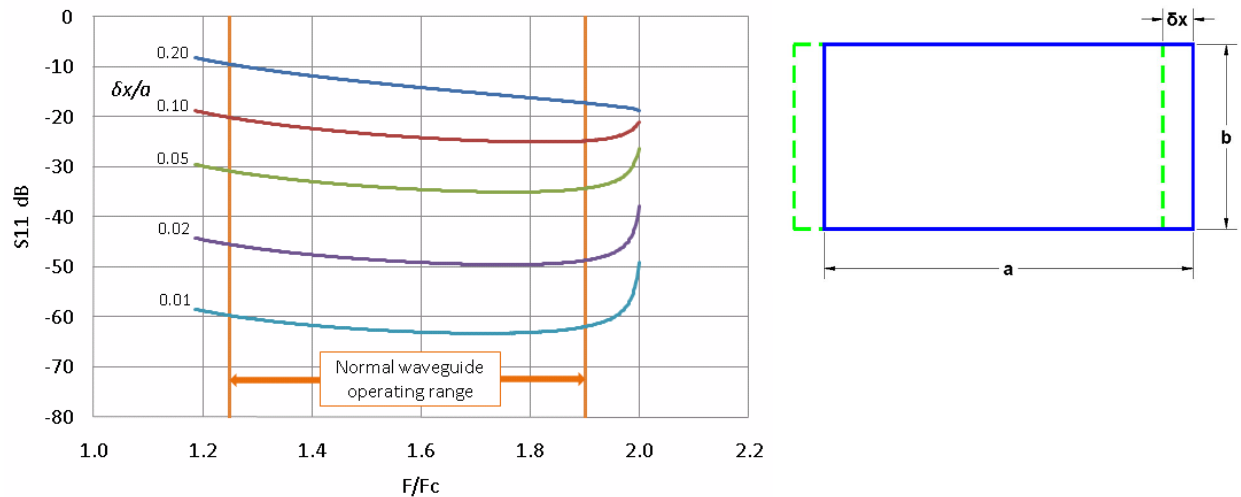


Fig. 4. Effect of flange misalignment parallel to the  $a$ -direction, for rectangular waveguides with 2:1 aspect ratio.

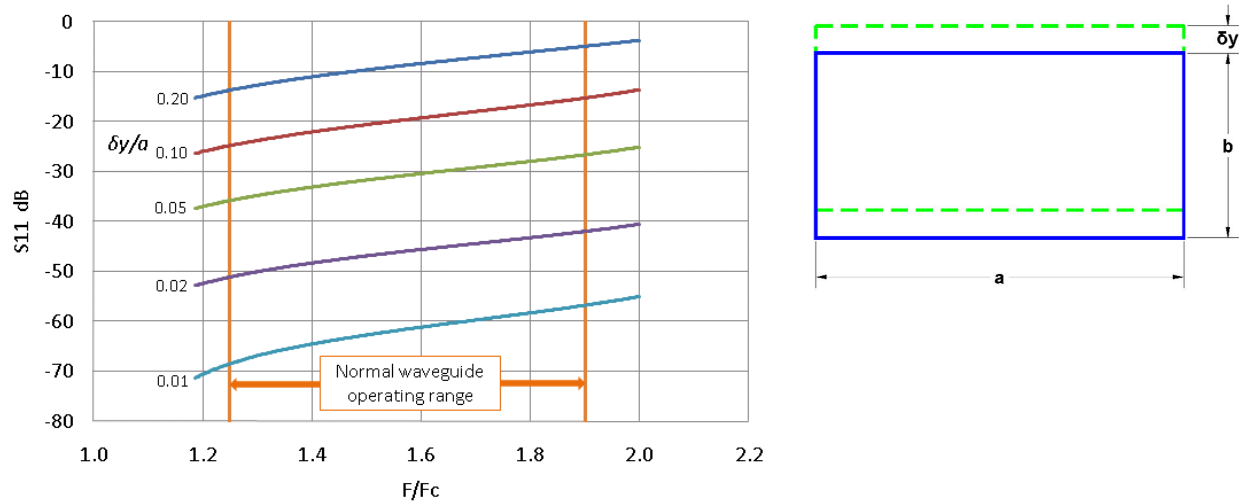


Fig. 5. Effect of flange misalignment parallel to the  $b$ -direction, for rectangular waveguides with 2:1 aspect ratio.

To first order, a misalignment in the  $a$ - or  $b$ -direction is equivalent to a frequency dependent shunt susceptance at the plane of the waveguide junction. For a misalignment in the  $x$ -direction the susceptance is negative (inductive), and for a misalignment in the  $y$ -direction the susceptance is positive (capacitive). This is evident in Fig. 6 which shows S11 as a function of frequency for misalignments of  $0.2a$  in the  $a$ - and  $b$ -directions.

For a misalignment with components in both the  $a$ - and  $b$ -directions, the opposite susceptances tend to cancel one another; this is shown in Fig. 6 for a diagonal misalignment with  $\delta x = \delta y = 0.2a$ .

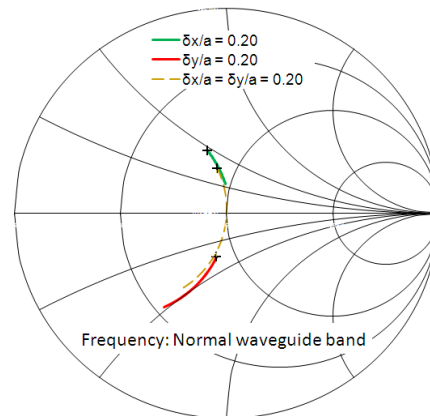


Fig. 6. Smith chart plot of S11 for misalignments  $\delta x = 0.2a$  (green),  $\delta y = 0.2a$  (red), and  $\delta x = \delta y = 0.2a$  (orange). Markers (+) indicate the low-frequency end of each curve.

### **Effect of angular flange misalignment**

It was shown in [3] that rectangular waveguides are quite tolerant to angular misalignment. Fig. 7 shows the reflection coefficient of a pair of waveguides for several angular misalignments. For a pair of UG-387 flanges with the standard pin and pin-hole sizes and location tolerances, the maximum angular misalignment is  $1.4^\circ$ . The angular alignment of the more precise variants of the UG-387 flange, and other more precise flange designs, is generally less than  $1.4^\circ$ .

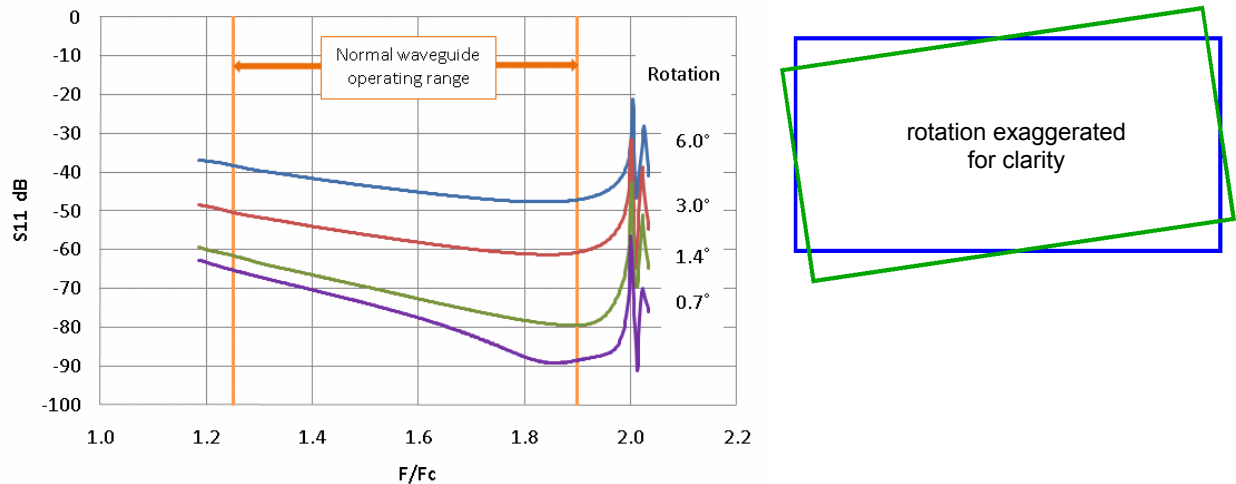


Fig. 7. Effect of an angular misalignment of rectangular waveguides with 2:1 nominal aspect ratio. The original UG-387 specification allows a maximum angular misalignment of  $1.4^\circ$ .

## References

- [1] D. J. Bannister, E. J. Griffin, and T. E. Hodgetts, "On the Dimensional Tolerances of Rectangular Waveguide for Reflectometry at Millimetric Wavelengths, NPL Report DES 95, September 1989.
- [2] M. M. Brady, "Cutoff wavelengths and frequencies of standard rectangular waveguides," *Electronics Letters*, vol. 5, no. 17, pp. 410-412, 21 Aug 1969.
- [3] A.R. Kerr, E. Wollack, and N. Horner, "Waveguide Flanges for ALMA Instrumentation," ALMA Memorandum 278, 9 Nov. 1999. <http://www.alma.nrao.edu/memos/html-memos/alma278/memo278.pdf>.

## Revision Notes

Original EDTN 215, 7 December 2009.  
 Revised 11 January 2010: Added Figs. 5 and 6 and related discussion.