#### NATIONAL RADIO ASTRONOMY OBSERVATORY GREEN BANK, WEST VIRGINIA

### ELECTRONICS DIVISION TECHNICAL NOTE NO. 168

MEASUREMENTS OF OPTICAL FIBER TEMPERATURE Title: COEFFICIENT OF DELAY

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Date: January 25, 1993

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(August 1992 Update)

Measurements of Optical Fiber Temperature Coefficient of Delay

> Roger D. Norrod January 25, 1993

#### Summary

The purpose of this note is to document some measurements of delay temperature coefficient recently made on several types of optical fiber. These measurements were undertaken in order to better understand the causes of delay temperature sensitivity in analog optical fiber microwave links. A discrepancy was noted between published data and results measured with a round-trip phase measurement system operating on an antenna in Green Bank. It was found that one type of "tight-buffered" single-mode fiber has a temperature coefficient of approximately 60 ppm, while samples of other types of single-mode fiber and "loose-tube" optical cable have coefficients of less than 10 ppm. Since temperature coefficient data is not usually available from the cable manufacturer, for applications where the delay (phase) stability is important, users should select the type of fiber carefully, or measure the temperature coefficient of a sample.

#### Interferometer Round-Trip Measurement System

In 1988, as part of the installation of new receivers on the 85-foot Interferometer antennas in Green Bank, analog optical fiber microwave links were installed to transmit LO reference signals from the control room to the front-end boxes (FEB) and to transmit IF signals from the FEB to the control room. On the 85-3 antenna, used in the USNO VLBI network, a round-trip phase measurement system was implemented to measure changes in the delay between the control room and the FEB. Basically, this system sends a 500 MHz signal (used as a LO reference signal) to the FEB over an analog fiber link. A sample of this signal is returned over a second fiber link (multiplexed with the IF signals) to the control room. A HP vector voltmeter is used to compare the phases of the outgoing and returned 500 MHz signals and this data is recorded by the antenna control computer. The systems were further described by Jim Coe in EDIR 287 and EDTN 149.

Plots of the resulting data are routinely produced, scaled to one-way delay in picoseconds. Figure 1 shows three representative plots of the delay (\*), overlaid by the measured outdoor air temperature (T) scaled at 20 ps/°C. It is obvious that the delay variations are highly correlated with the outdoor temperature, and one would suspect that this is due to changes in the effective length of the fibers running from the base of the telescope to the FEB, since the majority of the cable length is buried 18 inches deep. EDTN 149 states that the aerial cable is 65 meters long, and delay through single-mode optical fiber is commonly quoted in the literature at 5  $\mu$ s/km. If we believe these values, the empirical T<sub>c</sub> of 20 ps/°C indicates the fiber delay is changing approximately 60 ppm/°C. However, JPL and other researchers have commonly quoted standard single-mode optical fiber T<sub>c</sub> at 10 ppm/°C. Since we plan to use analog optical fiber links on the GBT for IF and LO reference distribution, it was important to understand the causes of this discrepency.

#### Laboratory Measurements

Modern low-loss single-mode optical fibers consist of a silicate glass core (approximately 8  $\mu$ m diameter), covered with a silicate glass layer (approximately 125  $\mu$ m diameter and called the cladding) having a slightly lower index of refraction. The vast majority of the optical energy propagates in the core. Some manufacturers dope the core to elevate the core index (called "matched-cladding fibers" meaning the cladding index is that of silica), others dope the cladding (called "depressed-cladding fibers") to reduce the cladding index. The cladding is coated with an opaque substance to help protect the glass and to prevent crosstalk. All fibers we tested used a color-coded, ultraviolet-cured acrylate coating of 250  $\mu$ m diameter. Figure 2 illustrates the standard fiber construction.

The delay temperature coefficient of three optical cable samples were measured in the laboratory:

Sample 1 was an Optical Cable Co. four fiber cable, 130 meters long, similar to the aerial cables installed on the 85-foot antennas. Figure 3 is an excerpt from the OCC catalog, showing the cable construction. The acrylate coated fiber is covered with a 900  $\mu$ m diameter tight buffer layer, followed by a kelvar strength layer, and finally a 2.5 mm diameter elastomeric jacket. These fiber subcables are laid together with an overall PVC jacket. Two fibers in this cable were tested independently and then two fibers spliced in series, giving a total length of 260 meters, were tested. During the tests, a jumper of tightbuffered fiber 2.5 meters long with a Radiall low-reflection connector was fusion spliced on each end of the fiber tested.

Sample 2 was a spool of matched-cladding acrylate coated fiber 2930 meters long, supplied by Litespec, Inc. A jumper of tightbuffered fiber 2.5 meters long with a Radiall low-reflection connector was fusion spliced on each end.

Sample 3 was a 210 meter length of a six fiber, loose-tube, optical cable supplied by Sumitomo Electric Fiber Optics Co. Figures 4a and 4b are excerpts from the Sumitomo catalog. The fibers used in the Sumitomo cable were manufactured by Litespec (a corporation formed as a joint venture by AT&T and Sumitomo), and are similar to the fibers of sample 2. A jumper of tightbuffered fiber 2.5 meters long with a Radiall low-reflection connector was fusion spliced on each end of one fiber.

The test setup used to measure the temperature coefficient is shown in Figure 5. The network analyzer was used to measure the change in insertion phase near 1 GHz as the chamber holding the optical cable sample was changed in  $5^{\circ}C$  steps. The change in delay was calculated from the phase change using the equation:

$$\Delta \tau = \Delta \phi / 360 / f$$

where  $\Delta \phi$  is the phase change in degrees and f is the measurement frequency.

Table 1 and Figure 6 summarizes results for the 260 meter length of Sample 1. The average measured coefficient of 63 ppm/°C is consistent with the data obtained by the Interferometer round-trip phase measurement system.

Table 2 and Figure 7 summarizes results for Sample 2. The average coefficient of 8 ppm/°C is consistent with coefficients reported in the literature for standard single-mode fiber.

Table 3 and Figure 8 summarizes results for Sample 3.

#### Discussion of Results

It has been recognized for many years that the phase delay through optical fibers is sensitive to temperature, pressure, strain, and other physical stimuli [1], [2]. These effects have even been utilized to fabricate optical fiber sensors for physical quantities. There are several mechanisms by which the stimuli act on the delay: by changing the refractive index and/or the physical dimensions of the fiber, both diameter and length Each mechanism contributes to the total delay change, some with [3]. positive coefficients, others negative. The magnitude of the various contributions are affected by many things, including the thickness and composition of coatings or jackets on the fiber [4]. It has been suggested that the temperature sensitivity could be controlled by proper selection of Sumitomo has produced special low temperature coating materials [5]. coefficient fibers by using special coatings to control the balance of the temperature coefficient contributions. (The Sumitomo fibers tested here were not of the low-Tc type.) Researchers at SAO presented data at the January 1993 URSI meeting also showing that fiber coatings or jackets effect the temperature coefficient.

#### <u>Conclusions</u>

It appears certain that the tight-buffered fiber selected originally for the Interferometer has a temperature coefficient seven or eight times higher than that obtainable with standard loose-tube fiber. We have had loose-tube fiber on the 140-foot for a couple of years with no obvious problems, but I hope we can install loose-tube fiber on 85-3 in the near future where routine phase measurements can be obtained. This will allow us to look for unforeseen effects that could be harmful to future applications.

#### Acknowledgements

Brian Crouse did the laboratory measurements and Frank Ghigo supplied the Interferometer phase measurement data.

### TABLE 1 Optical Cable Co. Cable Test Results

Cable Length : 260 m (approximate)

Measured Delay : 1.26  $\mu$ s (4.8  $\mu$ s/km)

Measured Loss : 21 dB (includes Tx/Rx)

<u>T (°C)</u>	(°)
30	-79.4
25	-6.3
20	140.9
15	286.8
10	454.8
5	621.0

Slope of Linear Fit: -28.8 °/°C  $\Delta \tau$  : -79.9 ps/°C

Delay Temp Coeff =  $-79.9 \text{ ps/}^{\circ}\text{C} / 1.26 \ \mu\text{s} = -63 \text{ ppm/}^{\circ}\text{C}$ 

#### TABLE 2 LiteSpec Cable Test Results

Cable Length : 2965 m

Measured Delay : 14.4  $\mu$ s (4.9  $\mu$ s/km)

Measured Loss : 24 dB (includes Tx/Rx)

_φ (°)
-11.7
179.2
378.9
588.1
790.2
1004.9

Slope of Linear Fit: -40.7 °/°C  $\Delta \tau$  : -119 ps/°C

Delay Temp Coeff = -119 ps/°C / 14.4  $\mu$ s = -8.3 ppm/°C

TABLE 3 Sumitomo Loose-Tube Cable Test Results

Cable Length : 215 m

Measured Delay : 1.09  $\mu$ s (5.1  $\mu$ s/km)

Measured Loss : 20 dB (includes Tx/Rx)

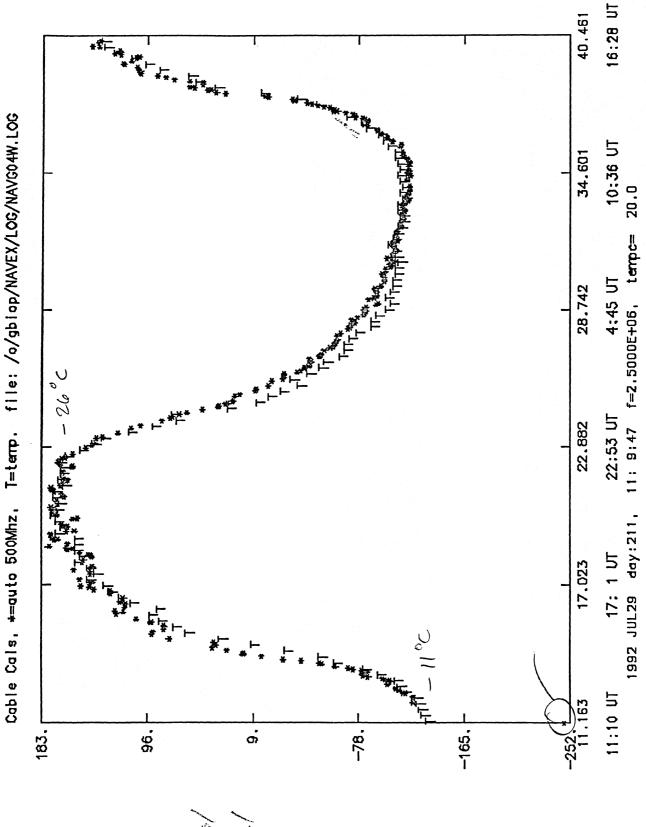
<u>T</u> (°C)	φ_(°)
-10	120.0
5	86.4
10	71.5
15	55.3
20	44.9
25	32.2
30	5.8

Slope of Linear Fit:  $-2.76 ^{\circ}/^{\circ}C$  $\Delta \tau$  :  $-7.9 \text{ ps/}^{\circ}C$ 

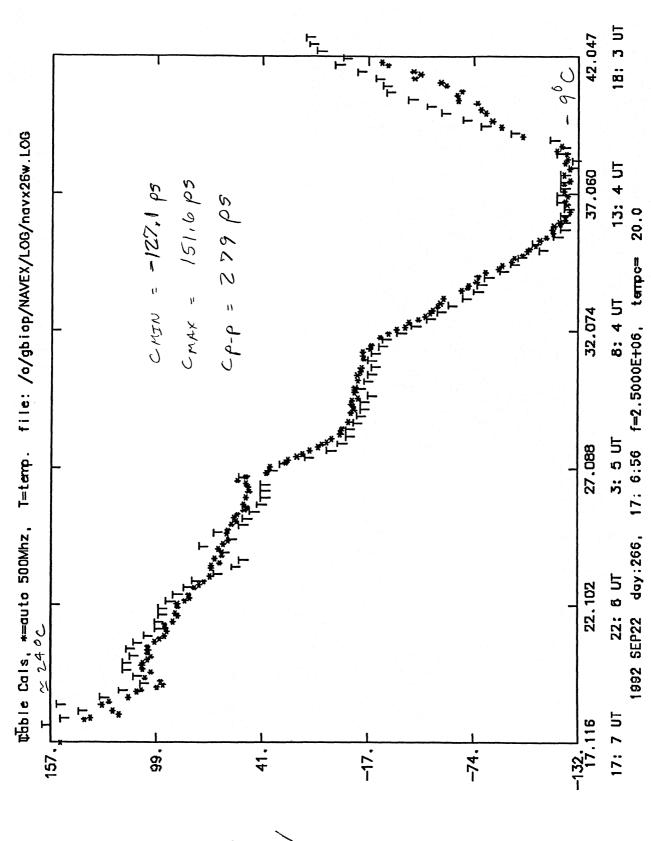
Delay Temp Coeff =  $-7.9 \text{ ps/}^{\circ}\text{C} / 1.09 \ \mu\text{s} = -7.3 \text{ ppm/}^{\circ}\text{C}$ 

#### References

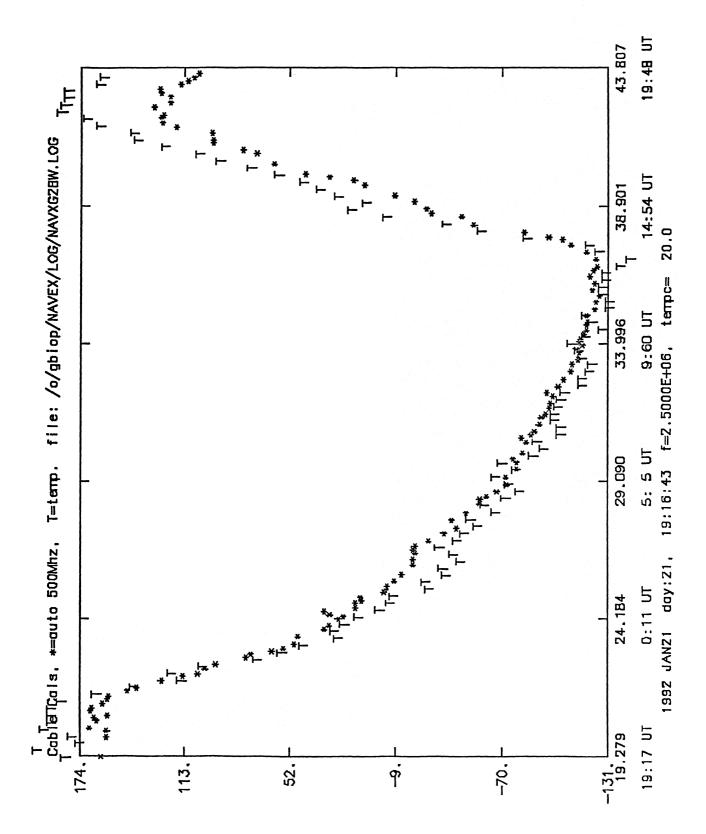
- [1] <u>Single-Mode Optical Fiber Measurement</u>,
   G. Cancellieri, ed. Artech House, 1993 Chapter 5.
- [2] Optical Fiber Sensors: Principles and Components, J. Dakin and B. Culshaw, Aertech House, 1988
- [3] "Fiber Optic Sensing of Pressure and Temperature",
   G. B. Hocker, Applied Optics, V. 18, No. 9, May 1979 pp 1445-1448.
- [4] "Temperature-induced Optical Phase Shifts in Fibers", N. Lagakos, J. Bucano, J. Jarzynsld, Applied Optics, V. 20, No. 13, July 1981, pp 2305-2308.
- [5] "Minimizing Temperature Sensitivity of Optical Fibers", N. Lagakos and J. Bucano, Applied Optics, V. 20, No. 19, October 1981, pp 3276-3278.

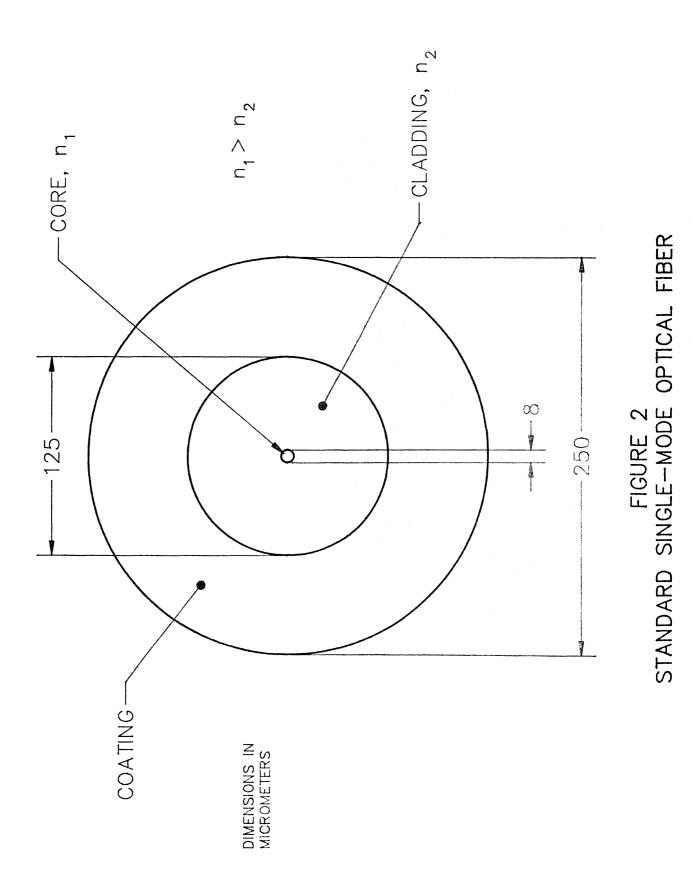


876%/ 4,4°C/



5865/ 2,9 °C/

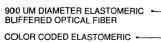




FROM Optical Cable Corporation Catalog

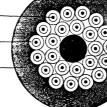
Figure 3

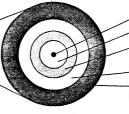
## SPECIFICATION GUIDE B-SERIES BREAKOUT CABLES



SUBCABLE JACKET

CORE-LOCKED™ PVC JACKET •





OPTICAL FIBER

- ACRYLATE FIBER COATING
   900 UM DIAMETER ELASTOMERIC
- BUFFERED OPTICAL FIBER
- ARAMID STRENGTH MEMBER (KEVLAR®)
   COLOR CODED ELASTOMERIC
- SUBCABLE JACKET

(DRAWINGS NOT TO SCALE)

BREAKOUT CABLE

SUBCABLE

	STANDARD (2.5 mm Subcable)				±		MINI n Subcable)	garra -	MICRO (1.5 mm Subcable)				
FIBER COUNT	Dia. (mm)	Wt. (kg/km)-		e Load Ig (N)* Long Term	Dia. (mm)	Wt. (kg/km)	Tensile Ratin Short Term		Dia. (mm)	Wt. (kg/km)		e Load g (N)* Long Term	
2	7.0	50	1,200	500	6.0	38	800	200	5.0	27	800	200	
4	8.0	65	2,000	800	7.0	50	1,600	400	6.0	37	1,600	400	
6	9.5	82	3,000	1,200	8.0	64	2,400	600	6.5	39	2,400	600	
8	11.0	111	4,000	1,700	9.5	83	3,200	800	7.5	52	3,200	800	
10	13.0	152	5,000	1,900	10.5	102	4,000	1,000	8.5	67	4,000	1,000	
12	12.5	148	6,000	2,500	10.0	96	4,800	1,200	8.0	64	4,800	1,200	
18	14.5	186	8,000	3,500	12.0	121	6,000	1,500	9.5	85	6,000	1,500	
24	17.5	237	10,000	3,800	14.0	178	7,200	1,800	11.0	108	7,200	1,800	
30	19.5	285	12,000	5,000	15.5	203	8,400	2,100	12.5	132	8,400	2,100	
36	20.5	305	14,000	6,000	16.5	208	9,600	2,400	13.0	137	9,600	2,400	
48	23.5	393	18,000	7,500	19.5	288	12,000	3,000	14.5	178	12,000	3,000	
60	25.0	426	22,000	8,800	20.5	305	14,400	3,600	15.5	194	14,400	3.600	
72	27.5	516	26,000	11,000	22.5	366	16,800	4,200	17.5	223	16,800	4,200	
84					24.5	433	19,200	4,800	19.0	254	19,200	4,800	
96	we reached man	files and a supervised			26.5	506	21,600	5,400	20.5	296	21,600	5,400	
108	1				27.0	509	24,000	6,000	21.0	301	24,000	6,000	
120				(N)		0.00			22.5	346	26,400	6,600	
132									23.5	377	28,800	7,200	
144		444							24.5	410	31,200	7,800	
156		1 Q	ana thatta						26.0	463	33,600	8,400	

SEE FIBER SPECIFICATION AND CABLE ORDERING GUIDE FOR FURTHER DETAILS

# SPECIFICATIONS COMMON TO ALL B-SERIES BREAKOUT CABLES

Minimum Bend Radius
Under Installation Tensile Load:
Under Long Term Tensile Load:
Operating Temperature:
Storage Temperature:
Crush Resistance:
Impact Resistance:
Flex Resistance:

20 x Outside Diameter 10 x Outside Diameter -40°C to +85°C -55°C to +85°C 2200 N/cm 2500 Impacts 2000 Cycles

These specifications are subject to change without prior notification.

Meets or exceeds BellCore requirements for intrabuilding fiber optic cables as outlined in TR-TSY-000409 and TR-TSY-000020.

# Loose Tube Cable Construction

# ► Typical Sumiguide Cable Construction

stranded around a fiber reinforced plastic

(FRP) or metallic center member, followed by a plastic binder. A water blocking jelly fills the

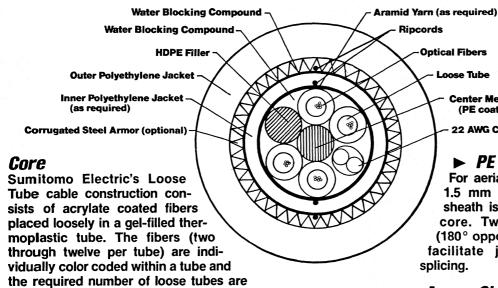
interstices of the cable core. For some cables

with an FRP center member (depend-

ing upon the number of tube positions),

aramid fiber is served over the core followed

by another polyester binder.



- Center Member (PE coated steel or FRP)

- 22 AWG Copper Pair (optional)

# ► PE Sheath

For aerial or duct applications, a 1.5 mm thick black polyethylene sheath is extruded over the cable core. Two ripcords are placed (180° opposed) under the sheath to facilitate jacket removal during splicing.

# Armor Sheath

For direct buried applications, the sheath consists of an inner jacket of black polyethylene. Two ripcords are placed 180° opposed under the inner jacket. A copolymer coated steel tape armor is longitudinally wrapped over the inner jacket for rodent resistance. This is followed by a black polyethylene outer jacket. A floodant is under the armor to prohibit water migration. Two ripcords are also placed (180° opposed) under the armor to facilitate jacket removal during splicing.

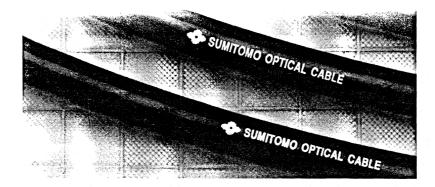
# of fibers	# of tube positions	# of fibers per tube	Metallic Center Member			r,	Di	electric Ce	enter Member		
			Nom Outei (mm)	S 12/100	Nom Wei (kg/km)		A STANDARD STATE	ninal r Dia. (in)	Nom Wei (kg/km)		
2-36	6	6	10.8	0.425	125	85	11.9	0.470	120	80	
37-48	8	6	12.5	0.490	160	110	13.2	0.520	155	105	
37-72	6	12	12.5	0.490	160	110	13.2	0.520	155	105	
73-96	8	12	14.5	0.570	210	145	15.3	0.600	200	135	
97-120	10	12	16.4	0.645	255	170	16.8	0.660	245	165	
121-144	12	12	18.4	0.725	315	215	19.0	0.750	305	205	

# Cable Diameter and Weights (Polyethylene Sheath)

# Cable Diameter and Weights (Steel Armor Sheath)

# of fibers	# of tube positions	# of fibers per tube	A REAL PROPERTY AND A REAL	Vetallic Cen	ter Membe	r	Di	electric Ce	nter Memb	er
				ninal r Dia. (in)	Nom Wel (kg/km)		Norr Outer (mm)		Nom Wei (kg/km)	
2-36	6	6	13.8	0.540	260	175	14.6	0.575	260	175
37-48	8	6	15.5	0.610	315	215	16.1	0.631	310	210
37-72	6	12	15.5	0.610	315	215	16.1	0.634	310	210
73-96	8	12	17.5	0.690	380	255	18.0	0.709	375	255
97-120	10	12	19.4	0.764	455	305	19.4	0.764	430	290
121-144	12	12	21.4	0.840	530	355	21.7	0.854	520	350





SUMIGUIDE LOOSE TUBE OPTICAL CABLES are state-of-the-art optical fiber cables for use in long and short haul telecommunications systems. The cable offering may contain as many as 144 singlemode or multimode optical fibers, and a variety of sheath configurations for effective use in duct, direct buried or aerial environments.

Sumitomo Electric Fiber Optics Corp. has developed and produced optical fiber products in the United States since 1985. Our parent company, Sumitomo Electric Industries, Ltd., is an international leader in the fiber optics industry since 1974 and, together, we have built a worldwide reputation of excellence by supplying superior quality and reliable products offering long life.

Sumitomo's dedicated and innovative personnel are committed to excellence, and our state-of-theart facility in North Carolina enables research and manufacture of the finest fiber optic communications products in the world.

Exacting standards, rigorous quality assurance and leading edge technologies are evidence of Sumitomo's commitment to our customers.

# Loose Tube Cable Mechanical/ Environmental Design Specifications

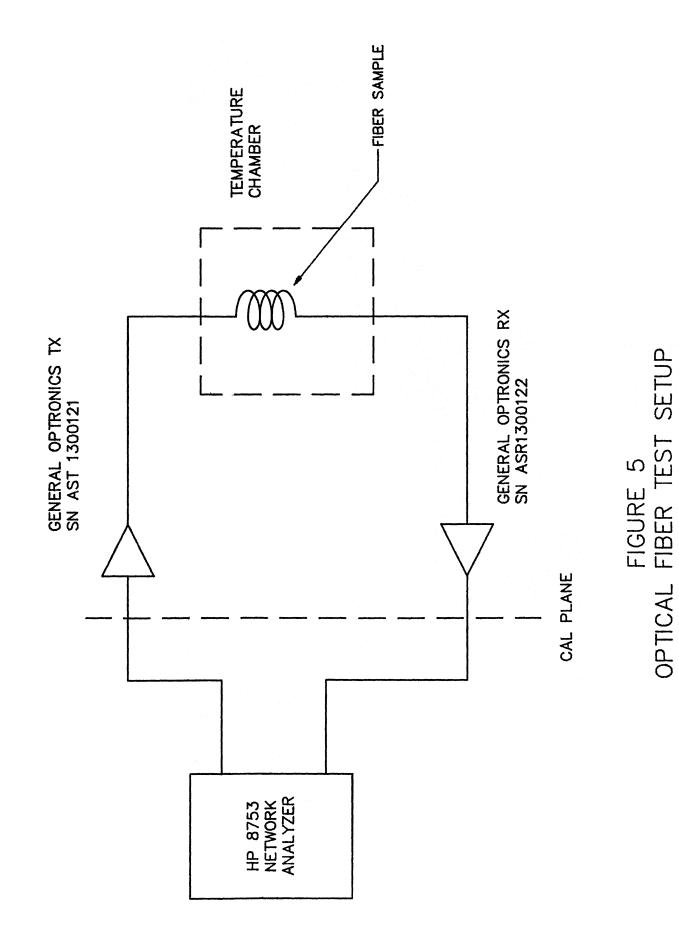
	Loose Tube				
Maximum Tensile Load During Installation (EIA RS-455-33)	5400N (1200 lb) Optional 2700N (600 lb) Standard				
Maximum Recommended Service Load (EIA RS-455-33)	1200N (270 lb) Optional 600N (135 lb) Standard				
Minimum Bend Radius During Installation After Installation	20 times cable diameter 10 times cable diameter				
Crush (EIA RS-455-41)	220N/cm for PE sheath 440N/cm for armor sheath				
Impact (EIA RS-455-25)	25 impacts				
Maximum Vertical Rise	< 50 meters				
Compound Flow Drip Temperature	65 °C				

SingleMode		. Ar sh	MultiMode	e State and State
Core Mode Field Diameter Mode Field Tolerance Core/Cladding Offset Optical Zero Dispersion Slope (So) Zero Dispersion Wavelength Maximum Dispersion @ 1310nm/1550nm Cutoff (cable)	50/125         62.5/125           Core Diameter $50 \pm 3\mu$ m $62.5 \pm 3\mu$ m           Numerical Aperture $0.20 \pm 0.02$ $0.275 \pm 0.02$ Core Non- Circularity $\leq 6\%$ $\leq 6\%$ Core Eccentricity $\leq 6\%$ $\leq 6\%$			
	Common Ch	aracteristics		
Cladding Cladding Diameter 125 ± 2µr Cladding Non-Circularity ≤ 29		250 ± 15µm UV Acrylate		50 KPSI Bend Radius 20mm Bend Radius 37.5mm

# ► Fiber Characteristics

# ► Transmission Characteristics

i i i i i i i i i i i i i i i i i i i	Single Mode	Mu	ıltimode	
	Maximum Attenuation (dB/km)	Maximum At	tenuation (dB/l	(m)
Grade	@ 1310/1550 nm	Attenuation Ranges	50/125	62.5/125
SA	0.35/0.25	@ 850nm	3.0	4.0
SB	0.40/0.30	@ 1310nm	1.0-1.5	1.0-1.5
SC	0.45/0.35	Bandwidth Ranges (M	Hz-km)	
SD	0.5/0.4	@ 850nm	200-400	160-200
SE	0.5/	@ 1310nm	400-1000	200-500



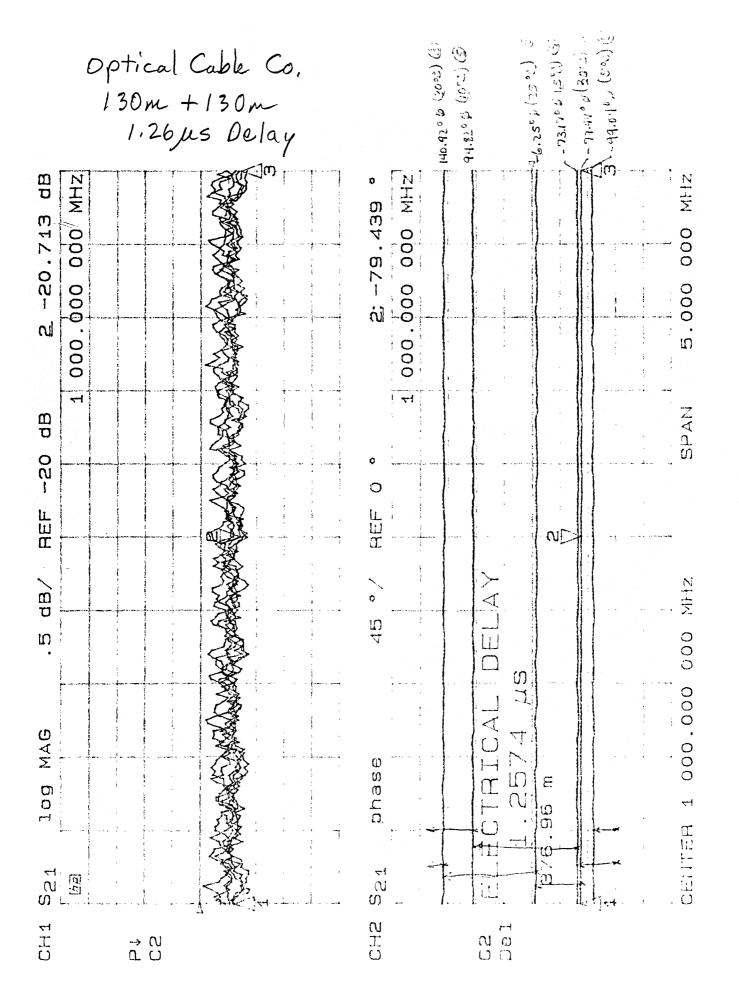
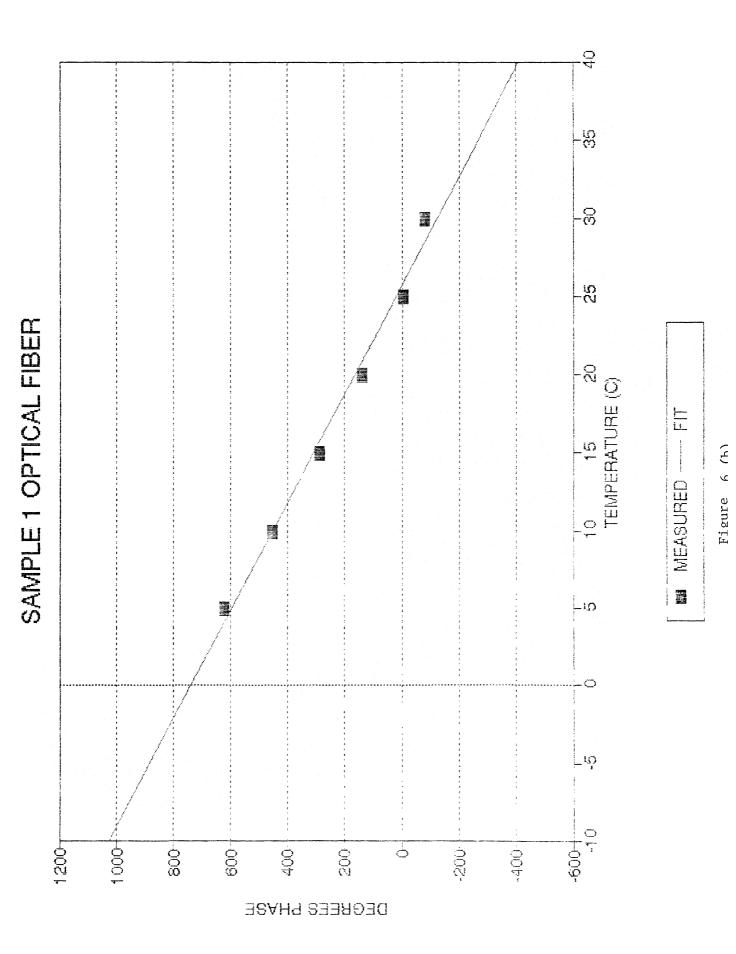


Figure 6 (a)



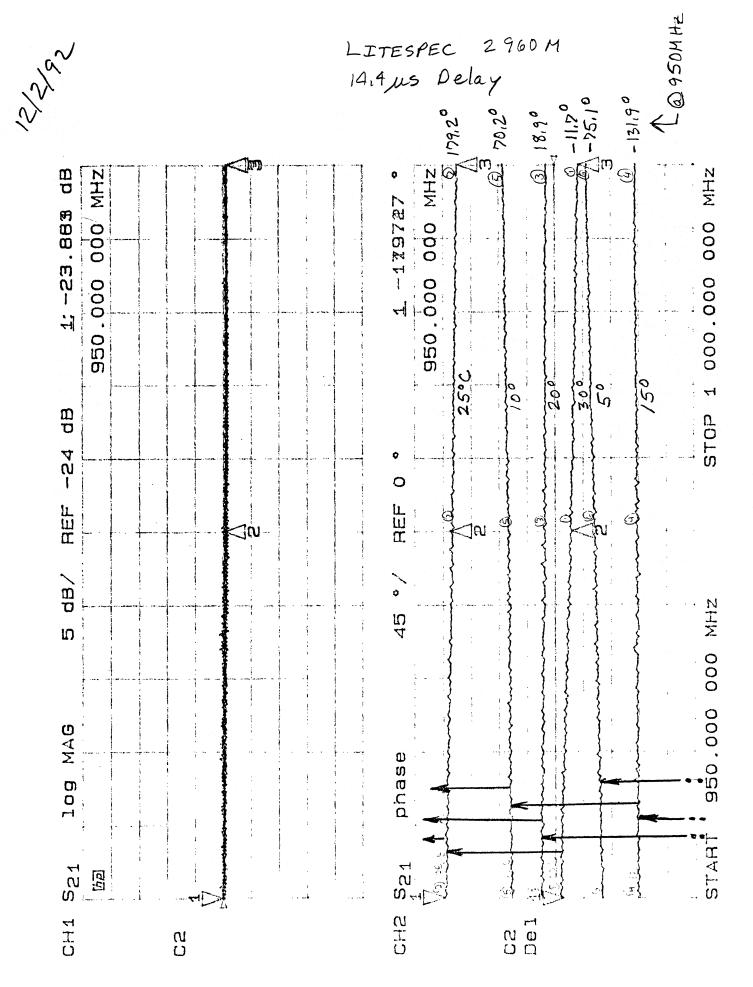
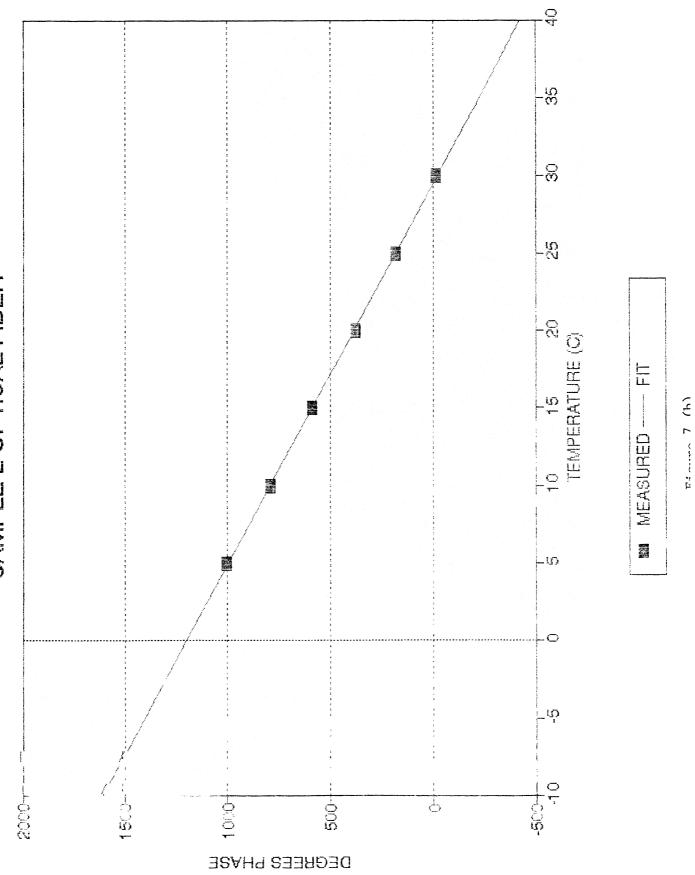


Figure 7 (a)



# SAMPLE 2 OPTICAL FIBER

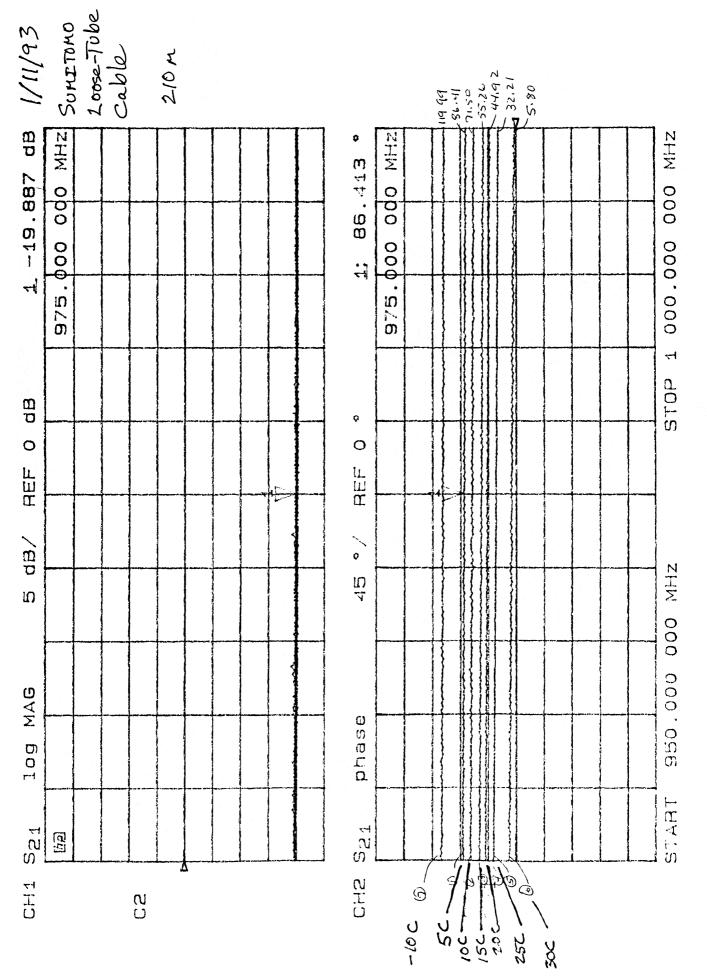
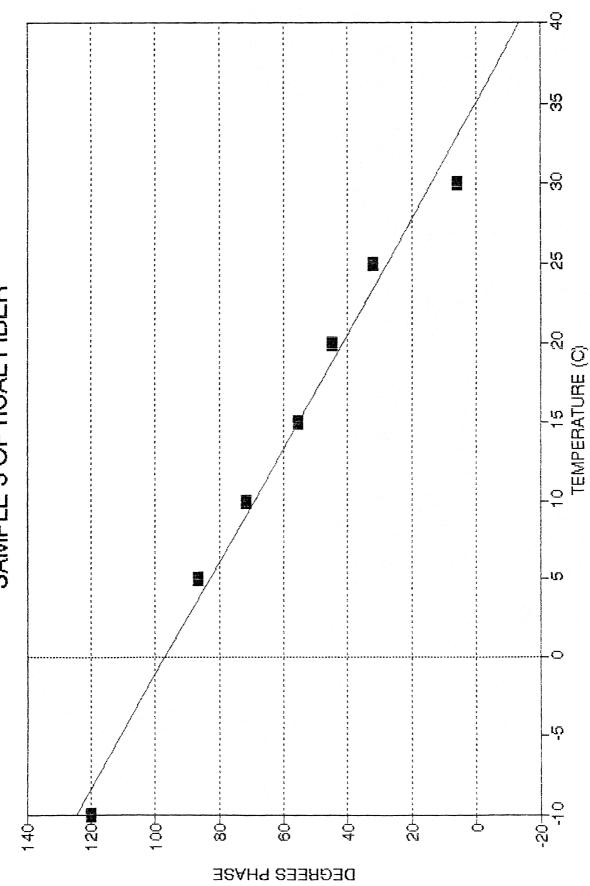


Figure 8 (a)



SAMPLE 3 OPTICAL FIBER

Finne R (h)

MEASURED -